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## Geographic information Features and Geometry - <br> Part 2: Measure

Information géographique -
Caractéristiques géographiques et géométrie -
Partie 2: Mesures

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## i. Abstract

The documents in this series named "Features and Geometry" describes how geographic information is stored as data using a "Feature Model" are structured, accessed, and manipulated. The most important property is "location" which is represented as geometry in the coordinates of a CRS associated to a datum. The basis for the coordinates is a datum surface which is usually represented as an oblate ellipsoid. The most likely datum is the one is associated to GPS location systems which are derived from the ellipsoid WGS84 (https://gisgeography.com/wgs84-world-geodetic-system/). All numeric examples in this document use WGS84, but the technology is not specific, and the values for the semiminor axis, semi-major axis and eccentricity can be adjusted for any reference ellipsoid.

This volume investigates accurate measurements of length and surface area on an ellipsoid. A metric is a function, system or standard of measurement. The curved nature of the ellipsoid does not support a simple "function-based metric" such as the Pythagorean metric on the plane nor the spherical metric on a sphere based on the central angle between two points.

On an ellipsoid, the curvatures of the surface changes with latitude ( $\varphi$ ), and the nature of latitude and longitude ( $\lambda$ ) differ also, so homogeneous functions such as used in the plane and the sphere do not work.

Spherical trigonometry is a rough approximation for the ellipsoid but in general do not take consideration scale which is dependent on latitude. Ellipsoidal geometry requires a Riemannian metric.
On an ellipsoid, the nature of the curvature at a point varies based on its relative position, and in the direction of the measurement. The Pythagorean metric on the plane, does work on the ellipsoid in small enough areas. The ellipsoidal metric takes (in a sense) both Pythagorean and spherical metric functions in small areas, and then calculate series of local measures and then combines them in summations (numeric integration).

## ii. Keywords

The following are keywords to be used by search engines and document catalogues.

| cartography | coordinate reference systems | curvature | radian |
| :---: | :---: | :---: | :---: |
| datum | differential geodesy | differential geometry | radius of curvature |
| ellipsoidal geometry | ellipsoidal metrics | first fundamental form | spherical geometry |
| geodesy | geographic database | geographic information systems <br> (GIS) | location |
| geography | geometry | measure, measurement, metric | numeric integration |

## iii. Preface

This document "Features and their geometry: Part 2 Measure" deals with metrics for geometry associated to a curved surface, ellipsoid, that approximates the earth's surface. The theory of the mathematics dates to Isaac Newton (calculus, circa 1670), Gauss and Riemann (differential geometry, circa 1826-1855). It is doubtful that any of the procedures applied here are currently under patents.

Recipients of this document are requested to submit, with their comments, notification of any relevant patent claims or other intellectual property rights of which they may be aware that might be infringed by any implementation of the standard set forth in this document, and to provide supporting documentation.

## iv. Submitting organizations

The organizations and individual members of the Simple Features SWG (standards working group) reviewed and commented to produce this Document to the Open Geospatial Consortium (OGC).
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## Features and Geometry - Part 2: Measure

## 1 Scope

This document describes how to measure length in meters and area in square meters of any curve or area on an ellipsoid (e.g. WGS84). Other ellipsoids may be used by adjusting the valued of the equatorial radius "a" and the polar radius "b" as appropriate. Ellipsoidal constants are kept in equations as variables; and can be used for any ellipsoid. Numeric examples use WGS84.
The only concept needed are numeric integration (4.13), radian (4.14) and radius of curvature (4.15).
The informative mathematics is in Annex A, and Annex B. The examples of the techniques for length and area are in Annex C.

### 1.1 Why this document is not a standard

This document describes the mathematics of the geometry described here as equations. This document informs anyone who implements these algorithms to measure geometries on the ellipsoid. The examples in the paper represented as tables were set up in spread sheets that would be simple loops in C++ or any programming language. Once a reasonable set of implementations are created; standards can then propose efficient interfaces to support the measured data.

### 1.2 Purpose

This document describes how measures of geometric objects on any ellipsoid (e.g. World Geodetic System 1984) are calculated, such as curves for length (in meters) and polygons for area (square meters). The WGS84 ellipsoid uses parameters in meters or ratios.
The measurements are not tied to a simplified representation as on a globe (a sphere) or on a map (a plane), but to the source of the data, e.g. the ellipsoidal coordinates of latitude ( $\varphi$ ) and longitude ( $\lambda$ ).

The equations and algorithms in this document work for any ellipsoid, but the numeric examples use WGS84 parameters. Angles (latitude and longitude) in calculations are in radians, because they easily convert angles in radians to arc distances in meters using the local radii of curvature Angles in examples, will normally be listed in both decimal degrees and radians, but calculations are in radians.

There are two type of radii that are required for measures.

- The radius of curvature of a parallel $\left(\rho(\varphi)=N(\varphi) \cos \varphi=a \cos \varphi\left(1-e^{2} \sin ^{2} \varphi\right)^{-0.5}\right)$ is in the plane of the parallel. The curvature is defined by the distance from the parallel to the polar axis. Because a parallel is a circle, the radius is constant along the parallel associated to its latitude, and only changes as the latitude changes. The radius at the equator is "a". The radius goes to 0 as the parallel nears the poles. See Figure 1 and Table 1.
- The radius of curvature of a meridian $\left(M(\varphi)=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-1.5}\right)$ is a function of latitude and varies from the equator (where the equatorial radius is "a") and decreases as the meridian approaches the pole (where the polar radius is "b"). The length of an arc (fixed as a angle) of latitude is longer in meters as the meridian approaches the poles. See Table 2.
The original definition of the Riemannian metric calculated these radii but used a different but valid method of calculating the radii of curvature. The equations in a Riemannian metric (A.3) are more
complex than the radius of curvature ( 4.1 and 4.15). The Riemannian calculations are more complex but numerically identical. Figure 1 gives a direct geometric picture of the curvature along a parallel, $\rho(\varphi)=N(\varphi) \cos \varphi$.

If points on a map are input, then the inverse projection from the map ( $\mathrm{x}, \mathrm{y}$ ) to the ellipsoid's latitude, longitude ( $\varphi, \lambda$ ) surface should be used [18]. Small map areas, as in an engineering drawing, where x and y are really a local Euclidean survey and probably not projected from ( $\varphi, \lambda$ ), then the usual Pythagorean metric suffices, and it does not require the formulae or methods here. The global metric needs the Pythagorean metric to be accurate "in small areas" (square kilometer, hectare) so that the summations (numeric integrals) presented below make that assumption. The local calculation to be "near-Euclidean" which require values of $\Delta \varphi$ and $\Delta \lambda$ be less than a degree to retain reasonable locally flat surface.

In addition to the 2 D surface metric there is a 3 D metric for a "near earth" use including latitude, longitude and elevation ( $\varphi, \lambda, h$ ) with respect to the ellipsoid (mean-sea level). This "near surface" has an advantage over the ECEF (X,Y,Z) which would have to have the ability to keep curves directly associated to the " $(\varphi, \lambda, h)$ " latitude, longitude and elevation point references involved, see [3], [4] and [19]. The algorithms for " $(\varphi, \lambda, h)$ " extend " $(\varphi, \lambda)$ " by adding elevation above the ellipsoid.
The numeric examples in this document will always follow the ellipsoidal surface ( $\mathrm{h}=0$ ). The extensions to the 2.5 D metrics in general use simple extensions to the 2D examples.

The circumference of a circle of radius " r " is " $2 \pi r$ ", any arc along a circle whose length equals the radius " r " is called a radian (approximately $57.295779513 \ldots{ }^{\circ}$ ). The arc length of a 1 radian angle is " r " and the arc length of $1^{\circ}$ is $\mathrm{r} / 57.295779513$ or 0.017453292519968 r . A radian is a ratio of arc length to arc length and represented in equations as unitless measures (a ratio).

### 1.3 The importance of numeric integration

The formulae for calculating distances and areas on an ellipsoid would seem to require some integral calculus (see Annex B). The problem is that almost all the integrals do not have simple solutions. For this reason, in an application environment where the length or area of a feature is required to support some accuracy (we try for centimeter level accuracy in our examples). Annex B shows some simple numeric approximations to the needed values. Isaac Newton (1643-1727) or Leibniz (1646-1716) use a similar approximation technique to what he called the integral of a function:

$$
\begin{aligned}
a & =x_{0}<x_{1}<\ldots<x_{n}=b ; \Delta x_{i}=x_{i}-x_{i-1} \\
\int_{a}^{b} f(x) d x & =\lim _{\substack{\Delta x \rightarrow 0 \\
n \rightarrow \infty}} \sum_{i=1}^{n}\left(\frac{f\left(x_{i}\right)+f\left(x_{i-1}\right)}{2}\right) \Delta x_{i} * * * \text { Trapdezoid Rule } \\
\int_{a}^{b} f(x) d x & =\lim _{\substack{\Delta x \rightarrow 0 \\
n \rightarrow \infty}} \sum_{i=1}^{n} f\left(x_{i}\right) \Delta x_{i} \quad * * * \text { Newton's definition }
\end{aligned}
$$

Eq 1.

The first technique represented above for the formulae above is called the "trapezoid rule" or "trapezium rule" for numeric integration which converges faster than the second approach "rectangular" which is the original form from Newton's definition. It is the purpose of this document is to use numeric integration while preserving accuracy in the answers while keeping the programs (a
loop for the summation) simple and sufficiently accurate for GIS use, with the value of the area under the function approximated with smaller and smaller polygonal sides.

Another technique called "Simpson's Rule" can be more accurate for a set of ( $\Delta x_{i}$ ), uses a parabolic approximation. In both techniques, as the maximum $\Delta x_{i}=\left|x_{i}-x_{i-1}\right|$ tends to zero, the numeric approximation to the integral $\int_{a}^{b} f(x) d x=\lim _{\substack{\Delta x \rightarrow 0 \\ n \rightarrow \infty}} \sum_{i=1}^{n} f\left(x_{i}\right) \Delta x_{i}$. See Table 2

The integrals we use comes from Gauss (1775-1855) and Reimann (1826-1866) in the 1850's to use integrals on ellipsoidal surfaces for geometry lengths and area (see Annex B). The key to accuracy of these summation loops is knowing how $\Delta \varphi$ and $\Delta \lambda$ measures are locally scaled to meters, by use of angles in radians and the appropriate radii of curvatures for meridians and parallels.


Figure 1 - Reduced latitude " $\beta$ ", geocentric latitude " $\psi$ ", and geodetic latitude " $\varphi$ ". (larger eccentricity for emphasis)

### 1.4 The importance of the radius of curvature for calculating arc length

Each point " $\alpha$ " on a curve has a radius of curvature " $\mathrm{r}_{\alpha}$ " which defines the best fitting circle tangent to the curve at that point. Along that fitted circle, the arc length of an arc segment of a small local angle " $\Delta \alpha$ " (expressed in radians) starting at the point has a length along the full circle of " $2 \pi r_{\alpha}$ " and a local distance along the curve of " $\Delta \alpha r_{\alpha}$ ". The "small arc" length of the arc and the length of the curve are very close. So much so that if the arc is "circle-like" such as a parallel (a circle of constant latitude $\varphi$, good for the entire curve) or an ellipsoid meridian (an ellipsoid, very near a circle) which works quite accurately for an angle of less than a degree.

Eq 2.
Length of the normal:

$$
N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
$$

Eq 3. Radius of the parallel: $\quad \rho(\varphi)=N(\varphi) \cos \varphi=\frac{a \cos \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}$

Eq 4. Radius of the meridian: $\quad M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}$

In the figure below, the radius of the parallel is " $N(\varphi) \cos \varphi$ ", and the length of the line that defines latitude " $\varphi$ " from the surface of the ellipsoid to the polar axis is " $N(\varphi)$ ". The general equation for such a radius of curvature is in definition 4.1. Clynch [9] has a full description of these radii.

Eq 5. Meridian Distance $=\int_{\varphi}^{\varphi^{\prime}} M(\varphi) d \varphi$

Eq 6. Parallel Distance $=\int_{\lambda}^{\lambda^{\prime}} \rho(\varphi) d \lambda=\rho(\varphi) \Delta \lambda$ (if $\varphi$ is constant, e.g. along a parallel)

$$
\begin{gathered}
f(t)=(\varphi(t), \lambda(t)) \Rightarrow \\
\operatorname{dist}\left(p=f(t), p=f\left(t^{\prime}\right)\right)= \\
\int_{t}^{t^{\prime}} \sqrt{(M(\varphi(t)) \cdot \varphi(t))^{2}+(\rho(\varphi(t)) \cdot \lambda(t))^{2}} d t
\end{gathered}
$$

Eq 7. Length of a curve:

Eq 8. Area in a polygon

$$
\operatorname{Area}(A)=\iint_{A} M(\varphi) \rho(\varphi) d \varphi d \lambda
$$

The formulae for radii above are all that is needed to measure the length of short segments of arc of latitude and longitudes on the ellipsoid. The examples later imply use of arcs of length in of degrees $0.10^{\circ}$ to $0.25^{\circ}$.

The integrals in Eq 8 and Eq 9 are difficult to solve in any closed form, and so the best was to calculate in a computer is the use of numeric integration as shown below in Eq 9 and Eq 10.

$$
\begin{aligned}
& \operatorname{dist}\left(c(t):\left[t_{0}, t_{n}\right] \rightarrow(\varphi, \lambda)\right. \\
& \qquad \Delta \varphi_{i}=\varphi_{i}-\varphi_{i-1} ; \quad \Delta \lambda_{i}=\lambda_{i}-\lambda_{i-1}
\end{aligned}
$$

Eq 9.
Length of a curve: $\left[t_{0}, t_{1}, \ldots, t_{n}\right]=\left[\left(\varphi_{0}, \lambda_{0}\right), \ldots,\left(\varphi_{n}, \lambda_{n}\right)\right]$

$$
\begin{aligned}
& \operatorname{dist}\left(p, p^{\prime}\right) \cong \sum_{i=1}^{n} \sqrt{\left(\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right) \Delta \varphi_{i}\right)^{2}+\left(\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2}\right) \Delta \lambda_{i}\right)^{2}} \\
& \varphi_{i-0 . c}=\left\{\varphi_{0}, \ldots, \varphi_{c}\right\} ; \Delta \varphi_{i}=\varphi_{i}-\varphi_{i-1} ; i=1, \ldots, c ; \\
& \lambda_{j=0 . . r}=\left\{\lambda_{0}, \ldots, \lambda_{r}\right\} ; \Delta \lambda_{j}=\lambda_{j}-\lambda_{j-1} ; j=1, \ldots, r \\
& \Delta \lambda=\sum_{\substack{\Delta \lambda_{i} \\
\text { in area }}} \Delta \lambda_{i}
\end{aligned}
$$

Eq 10. Area of polygon:

$$
\begin{aligned}
A \cong & \sum_{i=1}^{8}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right)\left[\sum_{j=1}^{8}\left(\frac{\rho\left(\varphi_{j}\right)+\rho\left(\varphi_{j-1}\right)}{2} \Delta \lambda_{j}\right)\right] \\
\cong & \left.\cong \sum_{i=1}^{8}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right)\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2} \Delta \lambda\right)\right] \\
& \left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right) \text { Height of strip, } \Delta \varphi_{i} \text { in radians } \\
& \left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2} \Delta \lambda_{j}\right) \text { Length of strip, } \Delta \lambda_{j} \text { in radians }
\end{aligned}
$$

The final summation works best for $\Delta \varphi$ and $\Delta \lambda$ shorter that $0.25^{\circ}$ ( 0.004363323 radians). The calculation in tables $1,2,3$, and 4 , result in errors of less than a millimeter.

### 1.5 The importance of the radius of curvature for calculating lengths and areas

The length of coordinate axes in the ellipsoidal coordinates (e.g. latitude ( $\varphi$ ), and longitude ( $\lambda$ ) are measured as angles, such as degrees, or radians, are not directly connected to the length of the arcs involved in meters. This requires us to convert angular arcs to the length in meters. The key is that an angle in radians is a function of the local radius of curvature. On a circle, it would be perfect, but meridians are ellipsoids, and the radius of curvature changes slowly getting longer as the latitude approaches the equator. This is the general idea for the use of Riemannian metrics. Riemannian metrics can produce exact measures by using integrals. Since there are not closed forms for these metrics, it is easier to use numeric approximation which derives from the original definitions for integrals stated by Newton. Taking significantly small arcs and applying the "trapezoid rule for numeric integration", gives us highly accurate and easily programmed numeric integration. This works because locally the Earth is "nearly flat", and the radii of curvature changes locally very closely, e.g. $0.25^{\circ}$ arcs are nearly "a linear" rate of change in the local radius of curvature, both for latitude and longitudes. Which means the "trapezoid rule for numeric integration" is highly accurate in this sort of small areas. Examples in the
annexes show that our application works for long arcs, one case is $0^{\circ}$ to $90^{\circ}$ gives us accuracy on the general error budget of a millimeter or less. Once the length algorithms, the area ones are similarly accurate.

### 1.6 Geometry and describing the position of features

The positions of features are represented as geometry, stored mostly as collections of algebraic curves, either as points, curvilinear features or boundaries of areas because these are things a computer can process. All of the integrals in this paper and in differential geometry in general, result in loops that aggregates the lengths of short curves or areas of small polygons that are then combined to create very accurate length or area of features, by using the scale factors in the information in Annex A and Annex B in the integrals in B.1. These integrals mimic classical Euclidean geometry, with the understanding that even for a curved surface, an area almost infinitesimally small works as Euclid and Pythagoras thought they would and change only with a near infinitely large numbers of infinitesimals are summed. It works when we get to $\Delta \varphi$ and $\Delta \lambda$ values less that a degree or 0.0174532925 radians e.g. $\pi / 180$ radians, a radian is $(180 / \pi)^{\circ}=57.29577951308232^{\circ}$ or $\left.57^{\circ} 17{ }^{\prime} 44.80624^{\prime \prime}\right)$.

These integrals are not directly "solvable" using integral calculus, so we back-up to the "summation" approximations of numeric integration. Within a $1^{\circ} \varphi$ by $1^{\circ} \lambda$ square the scale for both latitude and longitude vary slowly, see Table 1 and Table 2 . In general, a $1^{\circ} \varphi$ by $1^{\circ} \lambda$ square can only nearly be considered "planar", especially away from the poles.

In all the numeric calculations in this document, the requirements of the mathematics are geodetic coordinates, ( $\varphi, \lambda$ ), expressed in radians as required for the definitions, for the $\Delta \varphi$ and $\Delta \lambda$, which use the local radius of curvature (in meters) $M(\varphi)$ (along a meridian treated as a curve) and $\rho(\varphi)$ along a parallel treated as a curve. These can be used to scale angles to meters: $M(\varphi) \Delta \varphi$ along meridians and $\rho(\varphi) \Delta \lambda$ along parallels.
Note that both scaling factors depend solely on latitude $(\varphi)$. These factors derive from the concept of the radius of curvature discussed in clause 1.4 below, which is the basis for spherical metrics, but can be used in small areas on the ellipsoid by using the local radii. First, think locally (using spherical metric based on the radii of curvature for the $\varphi$ and $\lambda$ axes (parallels and meridians). The elements of the Riemannian metric in Annex A and Annex B calculate local radii of curvature as defined in 4.1 and 4.15, but use different methods that approach them directly. Although the two approaches derive different formulae which are identical in value but different in form.

These curves and areas inherit their properties from both the coordinate space (an ellipsoid) from which they are collected and the underlying geometry of that space. In these processes, the implementors generally deal with one or more of 3 coordinate systems and their underlying spaces.

- $\quad E^{3}$ (ECEF Earth-Centered Earth Fix Cartesian, $(X, Y, Z)$ or $\left(X_{i}, \mathrm{i}=1,2,3\right) \rightleftarrows$
- $S^{2}$ : (spheroid, ellipsoid, sphere), geodetic $(\varphi, \lambda)$ or geocentric $(\psi, \lambda) \rightleftarrows$
- $\mathrm{E}^{2}: \operatorname{map}(x, y)$ or $(x, i=1,2)$

Of these systems, only the first (which is used in GPS systems) uses "standard Euclidean geometry" which implies a Pythagorean metric $\left(d=\sqrt{\sum \Delta x_{i}^{2}}\right)$, the square root of the sum of the delta-coordinates squared. The last two systems have metrics that differ in form from the Cartesian distance based on Pythagoras. There is no universal "equation-based" metric spheroidal distance or map distances with the corresponding scale, which represent real distances until the projection is mapped back to the
spheroid. For example, a north-south circumnavigation along a meridian is $40,007.862 \mathrm{~km}$ (see Table 2), and an east-west circumnavigation along the equator is $40,075.016 \mathrm{~km}$, (see Table 1)

Spherical trigonometry works well on a "sphere", but even the small eccentricity of reference ellipsoids will alter both the distance and area measurements. In the example above of circumnavigations can differs by about 70 kilometers. To a lesser extent, a degree of latitude will vary slightly along a meridian because of the eccentricity and because the differences in curvatures (both along the parallel and the meridians) is dependent on latitude. Because of the same flattening, the degree of latitude also varies but only slightly ( 1.121 km ); 110.574 km at the equator and 111.694 km at the pole for a distance difference between the equator and the pole of only about $1 \%$.

Some maps can often use the standard Pythagorean metric for relatively small areas, such as engineering drawings over relatively small areas. The smaller area maps can get away with it because at that size the micro-geometry works as Euclid visualized it. These engineering drawings are not projection and therefore not really a topic for this paper.

Metrics on curved surfaces (such as an ellipsoid) embedded in $\mathbb{E}^{3}$ inherit a Riemannian metric from that embedding. Distance on a curved surface between two points $\mathrm{P}_{1}$ and $\mathrm{P}_{2}$ is the length of the shortest curve (the geodesic) on the surface that begins at $\mathrm{P}_{1}$ and ends at $\mathrm{P}_{2}$. If the surface is a plane, the derived metric is Euclidean. However, if the surface is curved, such as the ellipsoid, to get an accurate distance along the geodesic there are two options, both involving the curves that link the two points. The length of the shortest curve on the surface is the "distance" between the points. Once this curve is identified, the length of the curve is an integral, either in $\mathbb{E}^{3}(\mathrm{X}, \mathrm{Y}, \mathrm{Z})$ or on the spheroid $\mathbf{S}^{2}(\varphi, \lambda)$. As long as the representation of the $\mathbb{E}^{3}$ version of the curve fits the $S^{2}$ version of that same curve, the result will be the same (possibly with slightly different round-off errors).

The Earth-Centered Earth-Fixed Cartesian coordinate space ( $\mathbb{E}^{3}$ ) places the center of the ellipsoid or spheroid at the origin $(X, Y, Z)=(0,0,0)$, where the Greenwich Meridian $(\lambda=0$; longitude) as a curve on the spheroid that passes through the positive X -axis and is contained in the half plane where $\mathrm{Y}=0$. The Y -axis plane is $90^{\circ}$ East and the Z-axis is the rotational axis, and the positive $\mathrm{Z}+$-axis passes through the north pole.
This means the spheroid $\mathbf{S}^{2}$ is a topological sphere, with its center at the $\mathbb{E}^{3}$ origin, rotating about the Zaxis. Some systems ignore the eccentricity and use a sphere (mimicking a globe). This eccentricity was first hypothesized by Isaac Newton and was verified by measuring the distances between latitudes that would be equal on a sphere but different on an ellipsoid, further near the poles than near the equator. A grade measurement expedition (1735-1738) by the French Academy of Science to Lapland and Peru verified the oblateness. Later efforts by F. G. W. von Struve and Bessel in 1814 were used for the Bessel Ellipsoid (1841) with an inverse flattening of 299.1528 (WGS 1984 ellipsoid uses 298.2572).
A linear curve called a "line" taking it name from the formulae that in Euclidean (Cartesian) spaces is Euclid's line. But the algebra of the "line" segment between points $\vec{p}=\left(\varphi_{p}, \lambda_{p}\right)$ and $\vec{q}=\left(\varphi_{q}, \lambda_{q}\right)$ on a spheroid is simply a "linear" equation, using vector forms of $\vec{p}$ and $\vec{q}, \vec{c}(t):[0,1] \rightarrow S^{2}:[\vec{c}(t)=$ $(1-t) \vec{p}+t \vec{q}]$; the underlying surface gives lines a curvature. The geometry follows the surface of the coordinate space. The properties of the curve depend on both its algebra, and the way the coordinates are used to be associated to the Earth's surface. Flat maps tend to be used as if they were Cartesian (as defined by René Descartes (1596-1650)) and therefore aligned to Euclidean geometry. However, globes aren't Euclidean, they are either spheres modeled by spherical trigonometry or ellipsoids which are close to sphere, but not easily modeled until Gauss (1777-1855) and Riemann (1826-1866) used

Newton's (1642-1726) or Leibniz's (1646-1716) calculus to define "metrics" for other surfaces, not by equations but by integrals.

This standard enumerates the various mechanisms for representing feature positions as geometry on a curved surface spatially embedded in $\mathbb{E}^{3}$ or derived from such surfaces (e.g. map projections). The core difference between these geometries is the calculation of distances and associated lengths. Classical computer programs using coordinates work in Cartesian (and thereby Euclidean) coordinate spaces $\mathbb{E}^{2}$ and $\mathbb{E}^{3}$ which use a Pythagorean metric. Modern geodesy does its calculation generally in one of two manners: intrinsic or extrinsic metrics.

The intrinsic methods are based on operations on the surface being used, which usually involve differential geometry developed by Gauss and Riemann (most important the vector product) for curved space, usually creating integrals and not formulae for the calculation of lengths and areas (see Bomford [3] and Zund [38]). An example of a purely intrinsic method are the multiple measures of lengths of degrees of latitude and longitude which implied first spherical models and later with more data and more accurate data implied a spheroidal model (oblate spheroid).

The extrinsic methods take measures in a larger space and then interpret information about a surface embedded in this larger space ( $\mathrm{S}^{3}$ ). The best example is the GNSS satellite systems which interpret transmission time to multiple distance measures to calculate a position on the ellipsoid. In this later approach, the integrals can use the $\mathbb{E}^{3}$ coordinates $(X, Y, Z)$ and transform to geodetic coordinates $(\varphi, \lambda)$ i.e. latitude, longitude.

### 1.7 The importance of geodesy

Geodesy is the science of the shape and gravity of the Earth, specifically for the geospatial community, this has implications for the types of geometry embedded in geographic coordinate reference systems based on geographic datums and their reference ellipsoid. These coordinates expressed as positions on the ellipsoid, geoid or surface of the Earth involve positions defined with respect to the equator ${ }^{1}$, and the Prime Meridian (Greenwich) and "local vertical" offsets from that surface (elevation or depth). Once the coordinate system is defined, the geometry is expressed in that coordinate system, see ISO 19111 for the coordinate reference systems (CRS) and ISO 19107 for representing geometry in any coordinate systems. For example, the Euclidean line with all its properties cannot exist on a curved closed surface like a spheroid because the properties of such a surface prevent the fundamental infinities embedded in the concept of a line. A curve may seem to be a line in a small area, but the infinity of its length in Euclid's geometry cannot exist in a closed finite surface like a globe or an ellipsoid.

If a geographic representation system uses Euclidean geometry in $2 \mathrm{D}\left(\mathbb{E}^{2}\right.$ such as extrapolating from maps) or 3 D ( $\mathbb{E}^{3}$ either addition of elevation to an $\mathbb{E}^{2}$ system or embedding a 2D "Earth-like" (geoid) surface in an earth centered earth fixed coordinate system, ECEF), then they are engineering coordinate reference system $\left(\mathbb{E}^{2}\right.$ or $\left.\mathbb{E}^{3}\right)$ and should not to be confused with a projection where the

[^0]target coordinate space does not represent a surface with Cartesian, Euclidean and Pythagorean functions.

Because the Earth is not flat, the geometry of a geoid surface is non-Euclidean and all formulae on the plane that depend on Euclidean geometry, such as the Pythagorean Theorem, are usually invalid. There are several mechanisms that can be used to work around this, in differing order of functionality and software performance.

### 1.8 The importance of geometry on the ellipsoid

By our own common experience, if we are close enough to the earth's surface, Pythagorean metrics work. This is because that "close enough" looks like and works like a flat plane. So locally, the geometry is what we already know how it works. What differential geometry does is to "integrate" these small pieces into continuous realization of aggregating all the short parts with accurate where we add them to realize the length or areas, by aggregating all the little parts.
This leads to two problems: how do we convert latitude " $\varphi$ " and longitude " $\lambda$ " to meters (or feet). At the equator, we have almost 25,000 miles of longitude and at the poles we can stand on all the longitudes at $89^{\circ} 59^{\prime} 59.999^{\prime \prime}(\mathrm{N})$ latitude, is about 30 cm . The "parallel" radius of curvature the earth at $90^{\circ}-.001 "=89^{\circ} 59^{\prime} 59.999^{\prime \prime}$ is $\mathrm{r}=6,356,752.314245 \mathrm{~m}$; changing $.001^{\prime \prime}$ converted to radians, multiplied by $r$ to convert to meters is 30 cm . Geometry gives you the scales (local radius of curvature) that allow you to measure angles (latitude along meridians and longitude along parallels) in radians to meters $\mathrm{r}_{\varphi} \Delta \varphi$ and $\mathrm{r} \lambda \Delta \lambda$, in the direction of latitude or longitude; see clause 1.4.

## 2 Conformance Classes

A feature is a representation of a real-world object. For spatial applications, the most important properties of a feature are its location and shape. The most technically difficult part of geospatial application is dealing with the geometry that represents that location, usually on a map, ellipsoid or geoid. In small areas, Euclidean geometry work fine. However, the larger the area the greater the need to compensate for the Earth's curvature which can be dealt only with a non-Euclidean geometry engine.
The conformance classes in this document depend on the methods used for operations for geometry objects used for the spatial extents of features.
3D ECEF: 3D Earth Centered Earth Fixed: Use an appropriate ellipsoid and convert all coordinates to $\mathbb{E}^{3}$ and use integration and differential equations to make calculations in $\mathbb{E}^{3}$. See Burkholder [4]. An ECEF coordinates system is a right-handed $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ coordinate system. The geometry of features must be contained on the reference ellipsoid.
Ellipsoidal Geometry: Use an oblate ellipsoid having a fixed equatorial radius " $r_{e}$ " or " $a$ ", a slightly smaller polar radius " $r_{p}$ " or " $b$ " and use an ellipsoidal metric from differential geometry consistent with the geoid's radii. See Ligas, Panou [27], Eisenhart [13], Hotine [16], Lund [24], Struik [29], Zund [38], and more specifically differential geometry.

## 3 References

The following normative publications in their most recent form contain information important to this document.

OGC-17-087r10 Geographic information - Features and geometry - Part 1: Feature models
ISO 19101-1 Geographic information - Reference model
ISO 19103 Geographic information - Conceptual schema language
ISO 19107 Geographic information - Spatial schema
ISO 19108 Geographic information - Temporal Schema
ISO 19111 Geographic information - Spatial referencing by coordinates
ISO 19126: Geographic information - Feature concept dictionaries and registers
ISO/IEC 13249-3 - Information technology - SQL Multimedia and Application Packages - Part 3: Spatial
ISO 19162: Geographic information - Well-known text for coordinate reference systems

## 4 Definitions

In addition to the list below, any definition in any normative reference will be acceptable. All Standard English words are in either in the Oxford or Webster's dictionary, usually both, sometimes with variants in spelling. The better dictionaries of the English tend to list all allowable alternate spellings based on national usages and custom.

## 4.1 curvature (of a curve)

<differential geometry> second derivative of a curve parameterized by arc length, $\kappa$, at a point
Note to term: The curvature is the reciprocal of the radius of curvature (4.15)
Note to term: The radius of curvature of an arc is the radius of the best fitting circle of the curve at that point.

Eq 11. curvature of curve " c ":

$$
\kappa=\frac{c^{\prime \prime}}{\left(1+\left(c^{\prime}\right)^{2}\right)^{3 / 2}}
$$

See: Concise Dictionary of Mathematics, "curvature" [5]

## 4.2 ellipsoid reference ellipsoid

<geodesy> geometric reference surface represented by an ellipsoid of revolution, that is a surface of rotation around the polar axis so that the equatorial radii are all equal

## 4.3 ellipsoidal (geodetic) coordinate system

<geodesy> coordinate system in which position is specified by geodetic latitude, longitude and (in the three-dimensional case) ellipsoidal height

Note to term: Geodetic latitude is measured by the angular direction of the local normal to the equatorial plane. See Figure 1
[ISO 19111]

## 4.4 ellipsoidal geocentric coordinate system

<geodesy> coordinate system in which position is specified by geocentric latitude and longitude
Note to term: Geocentric latitude is measured by the direction of the line from the center ( $0,0,0$ ) in ( $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ ) of the ellipsoid to the surface.

## 4.5 ellipsoidal height, " $h$ "

<geodesy> distance above the reference ellipsoid along the local ellipsoidal principal normal
Krakiwsky [21], Clynch[8]

## 4.6 engineering coordinate reference system

coordinate reference system based on a local reference describing the relationship of points to a Euclidean coordinate system

Note to term: Any engineering coordinate system use a Euclidean metric, i.e. a subset of En usually at most 3 spatial and, optionally, 1 temporal.

## 4.7 first fundamental form (in differential geometry)

inner, dot or vector product on the tangent space of a surface in three-dimensional Euclidean space $\mathbb{E}^{3}$ which is derived canonically from the dot product (inner product) on the tangent space of a surface derived from the "vector dot product" in three- dimensional Euclidean space $\left(\mathbb{E}^{3}\right)$

Note to term: The first fundamental form is a Riemannian metric tensor usually derived from the embedding of the surface in $\mathbb{E}^{3}$. See [1] for tensors. The same mechanism can be used if the embedding is replaced with an isometry (a mapping which preserves distance). It is not necessary to change the extent of the metric. For example, the first fundament form for 3D polar coordinates should be functionally equivalent to standard polar coordinates used in physics $(\rho, \theta, \varphi)$, where $\rho$ is the distance from the origin, $\varphi$ is rotation from the x -axis towards the y -axis, and $\theta$ is rotation from the $\mathrm{x}-\mathrm{y}$ plane towards the z -axis.

Note to term: Alternatively, the first fundamental form can be derived by calculating the radius of curvature, (see 4.15)

See Annex B.

## 4.8 geodesy

scientific and technical discipline addressing the fundamental basis of positioning and localization of geographical information science that studies dimensions, shape and the gravity field of the Earth

Note to term: Both definitions above derived from IGN (translated from French). These definitions reflect both the purpose and the practice of geodesy. The purpose is to rationally locate positions on the earth which requires the practice of investigation of the shape and gravity of the planet (in this document, the Earth).

IGN [17]

## 4.9 geocentric latitude, $\Psi, \varphi^{\prime}, \varphi_{c}$, and sometimes, $\phi$ or $\varphi$

〈geodesy〉 angle to the equatorial plane of the line from the center of the ellipsoid to the surface of
the ellipsoid at the point referenced，positive north，negative south（in radians for the calculations in this document）

Note to term：Unlike geodetic latitude，the line that determines geocentric latitude passes through the geometric center of the ellipsoid but is not always perpendicular to the reference ellipsoid surface．

Krakiwsky［21］

### 4.10 geodetic latitude，$\varphi, \varphi \mathrm{g}$ ，and sometimes $\varphi$

〈geodesy，astronomy〉 angle that the normal at a point on the reference ellipsoid makes with the plane of the equator，positive north，negative south（in radians for the calculations in this document）

Note to term：The line that determines geodetic latitude is perpendicular to the reference ellipsoid and usually does not pass through the center of the ellipsoid，except along the equator or at the poles．The following are valid for the surface of the ellipsoid，where geodetic＂$\varphi=\varphi_{\mathrm{g}}$＂and geocentric＂$\psi=\varphi_{\mathrm{c}}$＂latitudes and＂$\lambda$＂longitude．

Eq 12．Geodetic latitude：$\varphi=\arctan \left[\frac{a^{2} \tan \psi}{b^{2}}\right]=\arctan \left[\left(1-e^{2}\right)^{-1} \tan \psi\right]$ i．e． $\tan \varphi=\frac{a^{2}}{b^{2}} \tan \psi$

Eq 13．Geodetic longitude：$\psi=\arctan \left[\frac{b^{2} \tan \varphi}{a^{2}}\right]=\arctan \left[\left(1-e^{2}\right) \tan \varphi\right] \quad$ i．e．$\quad \tan \psi=\frac{b^{2}}{a^{2}} \tan \varphi$

Note to term：If $\psi=\varphi$ then they are $0^{\circ}$ ，or $\pm 90^{\circ}$ ．The tangent at these angles has value of either 0 or $\pm \infty$ ．

Krakiwsky［21］

### 4.11 geoid

〈geodesy〉 equipotential reference surface of the Earth＇s gravity field which is everywhere perpendicular to the direction of gravity and which best fits a mean sea level either locally or globally
Note to term：Geoids are usually represented as differences from a reference See：Concise Dictionary of Mathematics，＂curvature＂［5］
ellipsoid．

### 4.12 metric，measure

function，system or set of algorithms that returns a numeric measure of some notional property such as distance or surface area，or any measured property possessed by an entity or set of entities
Note to term：In this document，the metric will speak to the measure of the length of curves or to the area of a surface．The basic units of measure in this paper will be the meter and square meter or aggreges of these such as kilometer or hectare（ 10,000 square meters）．

### 4.13 numerical integration

numeric methods to approximate values for definite integrals
Note to term: It may be that there is no analytical method of finding an antiderivative of the integrand. Among the elementary methods of numerical integration are the trapezoid rule or Simpson's rule.
See: Concise Dictionary of Mathematics, "numeric integration" [5]

### 4.14 radian (rad)

<mathematics> measure of an angle base on a portion of a circle, a full circle being $2 \pi$ radians,
Note to term: $\quad 1^{\circ}=0.01745329252$ radian $=\pi / 180^{\circ}$; 1 radian $=180^{\circ} / \pi=57.29577951^{\circ}$. So, an angle in degrees times $\pi / 180^{\circ}$ is converted to the same angle in radians.
Note to term: All integrals in this standard use radians as a measure of angle. The most important issue is the use of numeric integration where $\Delta \varphi$ and $\Delta \lambda$ will be expressed in radians, not in degrees. If the curve for $\Delta \varphi$ has a local radius of curvature of " $r \varphi$ " and similarly for $\Delta \lambda$, and a radius of curvature of the local $\lambda$-axis is " $r_{\lambda}$ " then the lengths of the arcs are approximately $r_{\varphi} \Delta \varphi=\operatorname{arclength}(\Delta \varphi)$ and $r_{\lambda} \Delta \lambda=\operatorname{arclength}(\Delta \lambda)$ dependent on the variations of the variance of the radius of curvature along the $\operatorname{arcs}$ of $\Delta \varphi$ and $\Delta \lambda$. If $\Delta \varphi$ and $\Delta \lambda$ are small enough (at least smaller than a degree), then the total length is:
Note to term: Tables may use two columns one for each angle; in degree ( ${ }^{\circ}$ ) and in radian (no unit of measure). Radians are considered a ratio, between a circular arc length and the corresponding radius of that circle. Since the "a" and "b" (the two axes length of the ellipsoid in meters) the result of any of the numeric integrals below will be in meters or squared meters.
Note to term: The radian appears in mathematical literature in 1871, but the concept derives from the middle ages, from Arabian mathematics.

### 4.15 radius of curvature

radius of the circle which best fits a curve at a point
Note to term: The radius of curvature is the reciprocal of the curvature (of a curve)4.1).
Eq 14. Radius of curvature: $\quad \rho=1 / \kappa$ where $\kappa=\frac{c^{\prime \prime}}{\left(1+\left(c^{\prime}\right)^{2}\right)^{3 / 2}}$

Note to term: If $\Delta \varphi$ and $\Delta \lambda$ are both less than 0.0043633231 radian ( .25 degree), the accuracy of the combined distances can have sub-meter or better accuracy (see radian (4.12) and Annex C). Zooming into smaller and smaller $\Delta \varphi$ and $\Delta \lambda$ will eventually produce better accuracy for the calculated arc length. The radius of curvature function along a parallel is $\rho(\varphi)=N(\varphi) \cos \varphi$ and along a meridian is $M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}$, see Eq 9 for the integral Eq 5 above, and the numeric integration in Table 2 below. Using
integral equations, the distance between longitudes in meters along the same latitude ( $\varphi$ ), the length of the interval $\left(\lambda_{0}, \lambda_{1}\right)$ is $\int_{\lambda_{0}}^{\lambda_{1}} \rho(\varphi) d \lambda$. The distance between latitudes along the same longitude $(\lambda)$, the interval $\left(\varphi_{0}, \varphi_{1}\right)$ is $\int_{\varphi_{0}}^{\varphi_{1}} M(\varphi) d \varphi$.
Note to term: If $\Delta \lambda_{n}=\left|\lambda_{n}-\lambda_{n-1}\right|$ were the two points are on the same parallel, i.e. are both the same " $\varphi$ ", then $\rho\left(\varphi_{n}\right) \Delta \lambda_{n}$ is the exact arc distance value in meters on the ellipsoid. If $\varphi_{\mathrm{n}}$ and $\varphi_{\mathrm{n}-1}$ are not equal, then a reasonable approximation between the two $\lambda$ 's is $\left[\frac{\rho\left(\varphi_{\mathrm{n}}\right)+\rho\left(\varphi_{\mathrm{n}-1}\right)}{2}\right] \Delta \lambda_{\mathrm{n}}$. The $M(\varphi) \Delta \varphi$ with a non-zero arc length for $\Delta \varphi_{n}=\left|\varphi_{n}-\varphi_{n-1}\right|$, then a reasonable approximation of the arc length for $\varphi$ is $\left[\frac{M\left(\varphi_{n}\right)+M\left(\varphi_{n-1}\right)}{2}\right] \Delta \varphi_{n}$. (see [32]).

Eq 15.
Delta Distance:

$$
\Delta d=\sqrt{\left(r_{\varphi} \Delta \varphi\right)^{2}+\left(r_{\lambda} \Delta \lambda\right)^{2}}
$$

Eq 16. Radius of Meridian:

$$
r_{\varphi}=M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}
$$

Eq 17. Radius of Parallel:

$$
r_{\lambda}=\rho(\varphi)=N(\varphi) \cos \varphi
$$

See: "curvature"

### 4.16 reduced latitude (of a point of latitude $\varphi$ ) parametric latitude $\boldsymbol{\beta}$

angle from the reference ellipsoid center to the point directly above the equator on the same line parallel to the polar axis of the point of latitude $\varphi$ on the reference ellipsoid to the point on the surrounding sphere.

Eq $18 . \quad$ Reduced latitude:

$$
\begin{aligned}
\beta(\varphi) & =\arctan \left(\sqrt{1-e^{2}} \tan \varphi\right) \\
& =\arctan ((b / a) \tan \varphi) \\
& =\arctan ((1-f) \tan \varphi)
\end{aligned}
$$

Note to term: $\quad$ Figure 1 shows the differences between both geodetic and geocentric latitude " $\varphi, \Psi "$ and the corresponding reduced latitude " $\beta$ ". The figure uses a larger eccentricity that would normally be seen on a reference ellipsoid
4.17 Riemannian metric $g(\vec{u}, \vec{v})=\vec{u} \cdot \vec{v} \in \mathbb{R}$
smooth function on a manifold M (e.g. surface) that defined a continuous inner product $g(\vec{u}, \vec{v})=\vec{u} \cdot \vec{v}$ (sometimes called the "dot product") at each point " $x$ " on the manifold on the tangent
spaces $T_{x}(M)$ at each point on $M$
Note to term: On an ellipsoid, $\mathrm{d}_{\varphi} \cdot \mathrm{d}_{\varphi}=\mathrm{M}^{2}(\varphi)$ and $\mathrm{d}_{\lambda} \cdot \mathrm{d}_{\lambda}=(\mathrm{N}(\varphi) \cos \varphi)^{2}$ and $\mathrm{d}_{\varphi} \cdot \mathrm{d}_{\lambda}=0$. The values of $\mathrm{M}(\phi)$ is the radius of curvature for the meridian at the latitude $\varphi$, and $N(\varphi) \cos \varphi$ is the radius of curvature for the parallel of latitude.

### 4.18 surrounding sphere (of the reference ellipsoid)

sphere centered at the origin of the reference ellipsoid with a radius equal to the ellipsoid's equatorial radius (semi-major axis "a").

## 5 Measure for an ellipsoidal ( $\varphi, \lambda$ ) coordinate systems and geometry

A radian has arclength " $r$ " on a circle of radius " $r$ ". The circumference is $2 \pi r=\pi \mathrm{d}$. All angles are expressed in radians.

1 radian $=57^{\circ} .295779513 \ldots=\left(180^{\circ} / \pi\right)$
Circle $=2 \pi=6.283185307 \ldots$
1 radian $=1 / 6.283185307 \ldots$ of the circle
1 degree $=\pi / 180=.017453292519943 \ldots$


The applications work with geometry in the standard geodetic coordinate system geodetic latitude ( $\varphi$ ), longitude ( $\lambda$ ), and ellipsoidal height, if needed, ( $\varphi, \lambda, h$ ). The following example deal with two corners of a latitude-longitude rectangle, with sides of two meridians and two parallels with two corners $\left(\varphi_{o}, \lambda_{o}\right)$ and $\left(\varphi_{1}, \lambda_{1}\right)$ with NS and EW distances are generally less than a quarter degree.

All angle in the equation for $\varphi, \lambda, \Delta \varphi$ and $\Delta \lambda$ are used in calculations in radians. All distance expressions along curves in ( $\phi, \lambda$ ) are in meters.
The north-south distance between 2 points, $\left(\varphi_{0}, \lambda_{0}\right)$ and ( $\varphi_{1}, \lambda_{1}$ ) projected on the same meridian $(\varphi)$ has a north-south distance of approximately:

Eq 19. NS distance: $\quad \operatorname{dist}_{n-s}=\left(\frac{M\left(\varphi_{0}\right)+M\left(\varphi_{1}\right)}{2}\right) \Delta \varphi=r_{\varphi} \Delta \varphi$ where $\Delta \varphi=\left|\varphi_{1}-\varphi_{0}\right|$.

The east-west distance between 2 points, $\left(\varphi_{0}, \lambda_{0}\right)$ and ( $\varphi_{1}, \lambda_{1}$ ) projected on the parallel $(\lambda)$ has an eastwest distance of approximately:

Eq 20. EW distance: $\quad \operatorname{dist}_{e-w}=\left(\frac{\rho\left(\varphi_{0}\right)+\rho\left(\varphi_{1}\right)}{2}\right) \Delta \lambda=r_{\lambda} \Delta \lambda$ where $\Delta \lambda=\left|\lambda_{1}-\lambda_{0}\right|$.

The distance between 2 points and the area of bounded rectangle $\left[\left(\varphi_{0}, \lambda_{0}\right),\left(\varphi_{1}, \lambda_{1}\right)\right]$ (

Eq 21. Combined distance: dist $=\sqrt{\left(r_{\varphi} \Delta \varphi\right)^{2}+\left(r_{\lambda} \Delta \lambda\right)^{2}} ;$ and area $=\left(r_{\varphi} \Delta \varphi\right)\left(r_{\lambda} \Delta \lambda\right)$

Are expressed in meters where $r_{\varphi}=\frac{M\left(\varphi_{0}\right)+M\left(\varphi_{1}\right)}{2}$ and $r_{\lambda}=\frac{\rho\left(\varphi_{0}\right)+\rho\left(\varphi_{1}\right)}{2}$. The length of a curve is calculated by Eq 104. The rectangle with the diagonal $\left[\left(\varphi_{0}, \lambda_{0}\right),\left(\varphi_{1}, \lambda_{1}\right)\right]$ has area $=\left(r_{\varphi} \Delta \varphi\right)\left(r_{\lambda} \Delta \lambda\right)$ in square meters. The area of a surface shall be calculated by equation Eq 96 . The radii of curvature for latitude and longitude are functions of $\varphi$, where " $a$ " is the equatorial radius and "e" is eccentricity; see 4.1.

Eq 22. Length of normal:

$$
N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
$$

Eq 23. Radii of longitude:

$$
\rho(\varphi)=N(\varphi) \cos \varphi=r_{\lambda}
$$

Eq 24. Radii of latitude:

$$
M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}=r_{\varphi}
$$

These radii can be taken to 14 significant digits, based on the lengths of the two radii of the ellipsoid, for the equatorial axis and polar axis. The flattening is also an algebraic function of the two ellipsoidal radii.

Eq 25.

$$
\text { Ellipsoid radii: } \begin{aligned}
& a=6,378,137.0 \mathrm{~m} \\
& b=6,356,752.314245180 \mathrm{~m}
\end{aligned}
$$

equator by definition
polar by calculation $b=a(1-f)$

The radii of curvature here depend on the two radii of the ellipsoid, which are defined by "exact values" means if the functions are taken as double precisions valid digits, the values of the above functions can be as many as 14 to 17 decimals digits. This class uses an $\mathbb{E}^{3}$, an Earth Centered Earth Fixed coordinate system where the reference ellipsoid is centered at the $(0,0,0)$ with the Z-axis containing the polar access, and the $\mathrm{X}-\mathrm{Y}$ plane containing the equator, and the intersection with the Greenwich " $0^{\circ}$ meridian" and the equator is on the X and Y -axis. Theses following lay out how geometry should be done on a reference ellipsoid, usually embedded in $\mathbb{E}^{3}$, in general the types of analytic surfaces use within a Datum.

Eq 26. Point: point $=\{(\varphi, \lambda)\}$

Eq 27. Curve: curve $=\left\{p_{i}=\left(\varphi_{i}, \lambda_{i}\right)\right\}=\left\{p_{0}=\left(\varphi_{0}, \lambda_{0}\right), p_{1}=\left(\varphi_{1}, \lambda_{1}\right), p_{2}=\left(\varphi_{2}, \lambda_{2}\right), \ldots, p_{n}=\left(\varphi_{n}, \lambda_{n}\right)\right\}$

$$
\text { surface }=\left[p_{i, j}=\left(\varphi_{i, j}, \lambda_{i, j}\right)\right]_{0,0}^{m, n}
$$

Eq 28. Surface:

$$
=\left[\begin{array}{ccccccc}
p_{0,0} & p_{0,1} & p_{0,2} & p_{0,3} & \cdots & p_{0, n-1} & p_{0, n} \\
p_{1,0} & p_{1,1} & p_{1,2} & p_{1,3} & \cdots & p_{1, n-1} & p_{1, n} \\
p_{2,0} & p_{2,1} & p_{2,2} & p_{2,3} & \cdots & p_{2, n-1} & p_{2, n} \\
p_{3,0} & p_{3,1} & p_{3,2} & p_{3,3} & \cdots & p_{3, n-1} & p_{3, n} \\
p_{4,0} & p_{4,1} & p_{4,2} & p_{4,3} & \cdots & p_{4, n-1} & p_{4, n} \\
\cdots & \cdots & \cdots & \cdots & \cdots & \cdots & \cdots \\
p_{m-3,0} & p_{m-3,1} & p_{m-3,2} & p_{m-3,3} & \cdots & p_{m-3, n-1} & p_{m-3, n} \\
p_{m-2,0} & p_{m-2,1} & p_{m-2,2} & p_{m-2,3} & \cdots & p_{m-2, n-1} & p_{m-2, n} \\
p_{m-1,0} & p_{m-1,1} & p_{m-1,2} & p_{m-1,3} & \cdots & p_{m-1, n-1} & p_{m-1, n} \\
p_{m, 0} & p_{m, 1} & p_{m, 2} & p_{m, 3} & \cdots & p_{m, n-1} & p_{m, n}
\end{array}\right]
$$

The simplest geometry figure is a point, a set of one position. Since within a point, there can be no motion without leaving, the point has zero-degrees of freedom (of motion) and is therefore referred to as a 0 -dimensional geometry. The next geometry up the scale of dimension is a curve. On a curve, motion along the curve has one degree of freedom and is therefore a 1-dimensional geometry figure. Following this pattern, surfaces are 2-dimensional, and solids are 3 dimensional. All geometry objects are sets of position and so every implementation of a geometry must have a manner to represent positions.

Measuring geometry, the array of $(\varphi, \lambda)$ pairs should coincide with the dimension of the geometry. In dealing with a point, only one control point is involved. In dealing with a curve, the sample points will be a sequential array of sample control points,

A geometry representation shall use a single coordinate reference system (CRS) to express position(s) in space. The CRS shall be consistent throughout any primitive object (point, curve, surface or solid). The geometry objects or datatypes shall contain an identifier for the CRS in use or inherit one from a container.

If the datum is dynamic, the CRS reference shall contain the epoch for which the coordinates are valid. The authority for a dynamic datum should be considered as the primary source of information concerning adjustment between epochs of the datum.
The application should be able to calculate the length and areas of feature geometries in the ellipsoidal coordinate system $(\varphi, \lambda)$ or $(\varphi, \lambda, h)$ based on integration either in $\mathbb{E}^{3}$ or on the ellipsoid using a first fundamental form for that ellipsoid. If the reference ellipsoid is a sphere, the application can use spherical trigonometry to calculate distances without using integration techniques. Using a sphere is inconsistent with the actual geometry, which is an ellipsoidal. Any geometric representation of feature position requires an understanding of the "rules" of the space where this geometry is created.

## 6 Geometry on a curved datum reference surface

This set of requirements lays out the requirements of doing geometry on a curved surface embedded in $\mathbb{E}^{3}$, in general the types of analytic surfaces use within a Datum, e.g. the reference surface or ellipsoid. See Burkholder [4].

The issue is that in $\mathrm{E}^{3}$ geometries are in coordinates in $(\mathrm{x}, \mathrm{y}, \mathrm{z})$ with the restriction stated in the above Measurements of distance or length, area or volume shall be equal with those that can be calculated on the reference ellipsoid using a Riemannian Metric (first fundamental form) (see 4.17) with a stated error budget. The values in the measurements are the local radii of curvature on the meridian and the parallel.

Note: The Riemannian metrics described Annex A works directly with geodetic coordinates, ( $\varphi, \lambda$ ); with geocentric coordinates $(\psi, \lambda)$. The geocentric system $(\psi, \lambda)$ is simpler, but the geodetic system $(\varphi$, $\lambda$ ) is more commonly used. Both systems are based on local radii of curvature (see Table 1 and 2 in Annex C).

The simpler geocentric system may be use in place of the more complex geodetic system by transforming $\varphi$ to $\psi$ and back as necessary, $\lambda$ remains the same in these transformations.
Geometry dependent on these systems such as geodesics (shortest distance), rhumb lines (constant bearing) and any geodesic circle (constant distance from a center point), shall be consistent with calculation in the Earth centered, Earth Fixed $\mathbb{E}^{3}$ coordinate system in which the datum surface is defined, with a stated error budget, and shall be consistent with the same geometries using ellipsoidal calculations in latitude ( $\varphi$ ) and longitude ( $\lambda$ ).

## 7 Geometry in map projection spaces with datum information

"It is possible to derive a set of formulae to convert geographic coordinates to grid coordinates in purely mathematical terms. In general, equations can be derived of the form. see [18] and [28].

Eq 29. $\quad$ Map position for $(\varphi, \lambda):(E, N)=f(\varphi, \lambda)$

Eq 30.

$$
\operatorname{Length}\left(\varphi_{s}, \varphi_{e}\right)=\int_{\varphi_{s}}^{\varphi_{e}} M(\varphi) d \varphi
$$

Eq 31. Lenght of a Merridian between $\varphi_{\mathrm{s}}$ to $\varphi_{\mathrm{e}}$ :

$$
\varphi_{s}, \ldots, \varphi_{e}=\varphi_{0}, \varphi_{1}, \varphi_{2}, \ldots, \varphi_{n} ; \Delta \varphi_{i}=\left|\varphi_{i}-\varphi_{i-1}\right|
$$

$$
d_{m}\left(\varphi_{s}, \varphi_{e}\right) \cong \sum_{i=1}^{n}\left(\frac{M\left(\varphi_{i-1}\right)+M\left(\varphi_{i}\right)}{2}\right) \Delta \varphi_{i}
$$

Eq 32. Length of a parallel from $\lambda_{s}$ to $\lambda_{\mathrm{e}}: \Delta \lambda=\left|\lambda_{e}-\lambda_{s}\right| \Rightarrow d\left(\lambda_{s}, \lambda_{e}\right) \cong \rho(\varphi) \Delta \lambda$

In other words, the position in a map space $(x, y)=(E, N) \rightarrow(\varphi, \lambda)$ is mapped to a position on the reference ellipsoid. The argument also implies a display or digital map should be associated to the map projection and which, a map or map-like display on a screen should be able to map back to geodetic coordinates

## 8 Numeric Integrals for Ellipsoidal Measures

### 8.1 Length of a Meridian Segment

Along a meridian, the radius of curvature is dependent on $\varphi$. See Table 2.

Eq 33. Exact Integral

Eq 34. Numeric Integral

$$
\begin{gathered}
\varphi_{0}<\varphi_{1}<\varphi_{2}<\ldots .<\varphi_{n} \\
\operatorname{Length}\left(\varphi_{0}, \varphi_{n}\right) \cong \sum_{i=1}^{n}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right) \Delta \varphi_{i}
\end{gathered}
$$

### 8.2 Length of a Parallel Segment

The radius of curvature for a parallel is dependent on the latitude of the parallel, and constant along the parallel.

Eq 35. $\operatorname{Length}\left(\lambda_{0}, \lambda_{n}\right)=\int_{\lambda_{0}}^{\lambda_{n}} \rho(\varphi) \cos \varphi d \lambda=\rho(\varphi) \cos \varphi\left|\lambda_{n}-\lambda_{0}\right|$

### 8.3 Length of a Curve

The definition of a curve on an ellipsoid (see ISO 19107 Geographic information - Spatial schema. A curve is defined by a set of segments points $=\left\{p_{0}=\left(\varphi_{o}, \lambda_{0}\right), p_{1}=\left(\varphi_{1}, \lambda_{1}\right) \ldots, p_{n}=\left(\varphi_{n}, \lambda_{n}\right)\right\}$ between each pair subject to an interpolation mechanism. For a numeric integral, it is easier to approximations using linear segments. If the curve is a line string the original data points can be used, but other curves should be densified by the interpolated points will allow to use a linear interpolation. This linear approximation even for complex curves works towards the correct measures.
In general, for two points on curve work better if the $\Delta \varphi$ if less than a quarter degree, and the difference between the line used in the numeric integration is relatively and is curve is quite small.
This suggests that a GIS metric system should include a "center point" function for each curve type, so that the line approximation can be used to support the accuracy needed for length digital integration.
For example, if we are dealing with $p_{0}=\left(\varphi_{o}, \lambda_{0}\right)$ and $p_{1}=\left(\varphi_{1}, \lambda_{1}\right)$ then there is a plane perpendicular to the line between $p_{0}$ and $p_{1}$ defines a surface perpendicular to the line between the two points, and the point on the curve that is in that surface e.g. $p_{0.5}$ between the two point that lies on the curve and is
approximately half way between $p_{0}$ and $p_{1}$. Continuing along the curve and introducing new half distance points along the curve, the difference between data points become closer to each other on the curve. Once the approximate distance between any two sequential points on the curve are within a quarter degree in both latitude $(\varphi)$ and longitude $(\lambda)$. Which approximates the distance between the two points as:

Eq 36. $\left|p_{i+1}-p_{i}\right| \cong \sqrt{\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i+1}\right)}{2}\right)^{2}\left(\Delta \varphi_{i}\right)^{2}+\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i+1}\right)}{2}\right)^{2}\left(\Delta \lambda_{i}\right)^{2}}$

In the equation below, the calculation of a curve length should be

$$
\begin{aligned}
\text { points } & =\left\{p_{0}=\left(\varphi_{o}, \lambda_{0}\right), p_{1}=\left(\varphi_{1}, \lambda_{1}\right) \ldots, p_{n}=\left(\varphi_{n}, \lambda_{n}\right)\right\} \\
\text { Curve } c(s) & =(\varphi(s), \lambda(s)) \\
\text { Lengtht }\left(p_{0}, p_{n}\right) & =\int_{0}^{t} \sqrt{\left(M(\varphi(s))\left(\frac{d \varphi}{d s}\right)\right)^{2}+\left(\rho(\varphi(s))\left(\frac{d \lambda}{d s}\right)\right)^{2}} d s \\
& =\lim _{\substack{n \rightarrow \infty \\
\Delta \rightarrow 0}} \sum_{i=1}^{n} \sqrt{\left(M\left(\varphi_{i}\right)\right)^{2}\left(\Delta \varphi_{i}\right)^{2}+\left(\rho\left(\varphi_{i}\right)\right)^{2}\left(\Delta \lambda_{i}\right)^{2}} \\
& =\lim _{\substack{n \rightarrow \infty \\
\Delta \rightarrow 0}} \sum_{i=1}^{n} \sqrt{\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right)^{2}\left(\Delta \varphi_{i}\right)^{2}+\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2}\right)^{2}\left(\Delta \lambda_{i}\right)^{2}}
\end{aligned}
$$

Eq 37.

The two variations use the original Newton's definition, and the later uses a trapezoid rule that makes a better local approximation because the ISO 19107 Geographic information - Spatial schema
Equations Eq 7 (curves) and Eq 8 (areas) are the integrals, and Eq 9 and Eq 10 are the numeric integrations of the integrals. The later approximations can be done to best that can be done in double precisions numbers. The tables below demonstrate this. See Table 2, Table 3 and Table 4.

## Annex A Descriptive values of an oblate ellipsoid

## A. 1 Ellipsoidal constants.

The following equations describe the important information of ellipsoids including geodetic coordinates $(\varphi, \lambda): \frac{X^{2}}{a^{2}}+\frac{Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}}=1$, where "a" is the semi-major axis (equatorial radius=6,378,137.0 m) and " b " is the semi-minor axis (the polar radius $=6,356,752.314245$ ). The inverse flattening is 298.257223563. Although all equations are valid for all ellipsoid, the numerical values are WGS84, the common spheroid for GPS.

Eq 38. Ellipsoid $\mathrm{S}^{2}$ (surface) and $\mathrm{D}^{3}$ (solid):

$$
S^{2} \Rightarrow \frac{X^{2}}{a^{2}}+\frac{Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}}=1
$$

$$
D^{3} \Rightarrow \frac{X^{2}}{a^{2}}+\frac{Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}} \leq 1
$$

Eq 39. $\quad$ Radii: $\quad \begin{array}{lll}a=6,378,137.0 \mathrm{~m} & \text { by definition } \\ b=6,356,752.314245180 \mathrm{~m} & \text { by calculation } b=a(1-f)\end{array}$

Eq 40. First eccentricity:

$$
e=\sqrt{\frac{a^{2}-b^{2}}{a^{2}}}=2 f-f^{2}
$$

Eq 41. Second eccentricity:

$$
e^{\prime}=\sqrt{\frac{a^{2}-b^{2}}{b^{2}}}
$$

Eq 42. Flattening:

$$
f^{-1}=\frac{1}{f}=298.257223563=\left(\frac{a-b}{a}\right)^{-1}=\frac{a}{a-b}
$$

Eq 43. First flattening:

$$
f=\frac{a-b}{a}=298.257223563
$$

Eq 44. Inverse Flattening:

$$
f^{-1}=\frac{1}{f}
$$

Eq 45. Second flattening:

$$
f^{\prime}=\frac{a-b}{b}
$$

## A. 2 Geodetic Ellipsoidal coordinates.

This clause shows that the standard mapping between geodetic $(\varphi, \lambda)$ and ECEF $(X, Y, Z)$ are consistent.

Eq 46. The ellipsoid surface:

$$
\frac{X^{2}}{a^{2}}+\frac{Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}}=1
$$

Eq 47. Length of Normal: $\left.N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=\frac{a^{2}}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}\right)$

Eq 48. Radius of Meridian; $\quad M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}$

Eq 49. $\quad \mathrm{X}$ in geodetic: $\quad X=N(\varphi) \cos \varphi \cos \lambda=\frac{a \cos \varphi \cos \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=\frac{a^{2} \cos \varphi \cos \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}$

Eq 50. Yin geodetic: $\quad Y=N(\varphi) \cos \varphi \sin \lambda=\frac{a \cos \varphi \sin \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=\frac{a^{2} \cos \varphi \sin \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}$

Eq 51. Z in geodetic: $Z=N(\varphi)\left(1-e^{2}\right) \sin \varphi=\frac{a\left(1-e^{2}\right) \sin \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=\frac{b^{2} \sin \varphi}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}$

Eq 52. Radius of parallel:

$$
\begin{aligned}
\rho(\varphi) & =\sqrt{X^{2}+Y^{2}} \\
& =\sqrt{N^{2}(\varphi) \cos ^{2} \varphi\left(\sin ^{2} \varphi+\cos ^{2} \varphi\right)} \\
& =N(\varphi) \cos \varphi=\frac{a \cos \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
\end{aligned}
$$

Eq 53. Coordinates:

$$
\begin{aligned}
& X=\rho(\varphi) \cos \lambda=\frac{a^{2} \cos \varphi \cos \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=\frac{a \cos \varphi \cos \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \\
& Y=\rho(\varphi) \sin \lambda=\frac{a^{2} \cos \varphi \sin \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=\frac{a \cos \varphi \sin \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \\
& Z=\frac{b^{2} \sin \varphi}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=\frac{a\left(1-e^{2}\right) \sin \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
\end{aligned}
$$

Thus, satisfying the ellipsoidal equation:

$$
\begin{aligned}
\frac{X^{2}+Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}} & =\frac{1}{a^{2}}\left(\frac{a^{4} \cos ^{2} \varphi\left(\cos ^{2} \lambda+\sin ^{2} \lambda\right)}{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}\right)+\frac{1}{b^{2}}\left(\frac{b^{4} \sin ^{2} \varphi}{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}\right) \\
& =\left(\frac{a^{2} \cos ^{2} \varphi}{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}\right)+\left(\frac{b^{2} \sin ^{2} \varphi}{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}\right) \\
& =\frac{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi} \\
& =1
\end{aligned}
$$

Burkholder [4], Bomford [3], Clynch [6], Hotine [16], IOGP[19], Jekeli [20], Krakiwsky and Thomson [21], Ligas [22], Panigrahi [26], Torge [31].

## A. 3 Geodetic Metric, Latitude ( $\varphi$ ) And Longitude ( $\lambda$ )

Using classical mathematical trigonometry, the above equations can be expressed, using geodetic latitude $\varphi$ and longitude $\lambda$. Taking the equations $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ expressed functions in geocentric coordinates, $(\varphi, \lambda)$. This is essentially the creation of the matrix of transformations $J\left(\frac{\mathrm{X}, \mathrm{Y}, \mathrm{Z}}{\varphi, \lambda}\right)$. Below, using geodetic latitude using the equations in the ECEF (GSDM), we calculate the $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ coordinates as functions of latitude and longitude, $(\varphi, \lambda)$. Taking derivatives with respect to both $\varphi$ and $\lambda$, we get the radius of curvature for the axes for both $\varphi$ and $\lambda$. The values come out squared, because what is derived is the dot products of the tangent vector, e.g. the squares of the radii of curvature.

Eq 55. Ellipsoid surface:

$$
\frac{X^{2}}{a^{2}}+\frac{Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}}=1
$$

Eq 56. Length of normal:

$$
N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=\frac{a^{2}}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}
$$

$$
N^{\prime}(\varphi)=\frac{a e^{2} \sin \varphi \cos \varphi}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}=\frac{a^{4} e^{2} \sin \varphi \cos \varphi}{\left(a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi\right)^{3 / 2}}
$$

Eq 57. Radius of Parallel:

$$
\rho(\varphi)=N(\varphi) \cos \varphi=\frac{a \cos \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
$$

Eq 58. Radius of Meridian:

$$
M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}
$$

Eq 59.

$$
\text { XYZ to elliptical: }\left[\begin{array}{l}
X \\
Y \\
Z
\end{array}\right]=\left[\begin{array}{l}
\frac{a^{2} \cos \varphi \cos \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=N(\varphi) \cos \varphi \cos \lambda=\frac{a \cos \varphi \cos \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \\
\frac{a^{2} \cos \varphi \sin \lambda}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=N(\varphi) \cos \varphi \sin \lambda=\frac{a \cos \varphi \sin \lambda}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \\
\frac{b^{2} \sin \varphi}{\sqrt{a^{2} \cos ^{2} \varphi+b^{2} \sin ^{2} \varphi}}=N(\varphi)\left(b^{2} / a^{2}\right) \sin \varphi=\frac{a\left(1-e^{2}\right) \sin \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}
\end{array}\right]
$$

This creates the components for the first fundamental form, which is a vector inner product for $\vec{u}$ and $\vec{v}$ in the vector space for the coordinates $(\boldsymbol{\varphi}, \boldsymbol{\lambda})$ whose vectors spanned by $(\overrightarrow{\boldsymbol{v}}, \overrightarrow{\boldsymbol{u}})$ as defined above. In other words, these are vectors for the coordinate space of $(\boldsymbol{\varphi}, \lambda)$ i.e. the reference ellipsoid. The inner product also implies that any vectors in the $\varphi$-direction at a point is always perpendicular to vectors in the $\lambda$-direction.

Geocentric measures are measured along a line from the center of the ellipsoid (origin of the coordinate system) to the point. Geodetic latitude makes things a bit more complex. A geocentric latitude is slope of the upward normal from the surface of the ellipsoid which is equal to the geocentric latitude at the equator and the poles.
Similar calculations for geodetic latitude are a bit more complicated. The equations for this form has been, often with slightly different variable names, around for quite a long time, See Bomford [3] (at least in the $3^{\text {rd }}$ and later editions), Burkholder [4], Hotine [16], IOGP[19], Jekeli [20], Krakiwsky and Thomson [21], Ligas [22], Panigrahi [26], Torge [31], Clynch [6], [7] and [8]. The differences in the various versions of the model were essentially in the choice of variable names, and the details on the calculations.

Eq 60. Reimann metric:

$$
\left.\left.\begin{array}{rl}
\mathrm{J}\left(\frac{X, Y, Z}{\varphi, \lambda}\right) & =\left[\begin{array}{ll}
\frac{\partial \vec{X}}{\partial \varphi}=d \varphi & \frac{\partial \vec{X}}{\partial \lambda}=d \lambda
\end{array}\right] \\
& =\left[\frac{\partial}{\partial \varphi}\left[\begin{array}{c}
\mathrm{N}(\varphi) \cos \varphi \cos \lambda \\
\mathrm{N}(\varphi) \cos \varphi \sin \lambda \\
\mathrm{N}(\varphi)\left(1-e^{2}\right) \sin \varphi
\end{array}\right] \quad \frac{\partial}{\partial \lambda}\left[\begin{array}{c}
\mathrm{N}(\varphi) \cos \varphi \cos \lambda \\
\mathrm{N}(\varphi) \cos \varphi \sin \lambda \\
\mathrm{N}(\varphi)\left(1-e^{2}\right) \sin \varphi
\end{array}\right]\right.
\end{array}\right]\right] \text { ( } \begin{aligned}
\left.\mathrm{N}^{\prime}(\varphi) \cos \varphi-\mathrm{N}(\varphi) \sin \varphi\right) \cos \lambda & -\mathrm{N}(\varphi) \cos \varphi \sin \lambda \\
& =\left[\begin{array}{cc}
\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-\mathrm{N}(\varphi) \sin \varphi\right) \sin \lambda & \mathrm{N}(\varphi) \cos \varphi \cos \lambda \\
\left(1-e^{2}\right)\left(\mathrm{N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right) & 0
\end{array}\right]
\end{aligned}
$$

Eq 61. $\quad$ Radii $\varphi, \lambda$ :

$$
\begin{aligned}
& \vec{u}_{1}=\frac{\partial \vec{X}}{\partial \varphi}=\left[\begin{array}{l}
\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-\mathrm{N}(\varphi) \sin \varphi\right) \cos \lambda \\
\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-\mathrm{N}(\varphi) \sin \varphi\right) \sin \lambda \\
\left(1-e^{2}\right)\left(\mathrm{N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right)
\end{array}\right]: \\
& \vec{u}_{2}=\frac{\partial \vec{X}}{\partial \lambda}=\left[\begin{array}{c}
-\mathrm{N}(\varphi) \cos \varphi \sin \lambda \\
\mathrm{N}(\varphi) \cos \varphi \cos \lambda \\
0
\end{array}\right]
\end{aligned}
$$

First fundamental form for geodetic coordinates $(\varphi, \lambda)$ :

Eq 62.

$$
E(\varphi)=a_{1,1}=\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-\mathrm{N}(\varphi) \sin \varphi\right)^{2}+\left(\frac{b^{2}}{a^{2}}\right)^{2}\left(\mathrm{~N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right)^{2}
$$

$E(\varphi):$

$$
\sqrt{E(\varphi)}=M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2}
$$

The equality $E(\varphi)=M^{2}(\varphi)$ has been checked numerically for $\pm 90^{\circ}$. An algebraic proof has been difficult to find. In essence, the calculations for $\sqrt{E(\varphi)}$ and $M(\varphi)$ are both valid calculations for a meridian's radius of curvature, e.g. $u_{1} \bullet u_{1}=\left|u_{1}\right|^{2}=(\text { radius of curvature })^{2}$.

Eq 63. $\quad F(\varphi)=0=a_{1,2}=a_{2,1}=0 ;\left[a_{i, j}\right]=\left[\vec{u}_{i} \cdot \vec{u}_{j}\right] ; \vec{u}_{i} \bullet \vec{u}_{j}=\vec{u}_{i}\left[a_{i, j}\right] \vec{u}_{j}{ }^{t}$

Eq 64. $\quad G(\varphi)=a_{2,2}=(\mathrm{N}(\varphi))^{2} \cos ^{2} \varphi\left(\sin ^{2} \lambda+\cos ^{2} \lambda\right)=\mathrm{N}^{2}(\varphi) \cos ^{2} \varphi=(\mathrm{N}(\varphi) \cos \varphi)^{2}=\rho^{2}(\varphi)$ The Riemannian metric is:

Eq 65.

$$
\left[a_{i, j}\right]=\left[\begin{array}{cc}
\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi+\mathrm{N}(\varphi) \sin \varphi\right)^{2}+\frac{b^{4}}{a^{4}}\left(\mathrm{~N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right)^{2} & 0 \\
0 & \mathrm{~N}^{2}(\varphi) \cos ^{2} \varphi
\end{array}\right]
$$

$$
=\left[\begin{array}{cc}
M^{2}(\varphi) & 0 \\
0 & \mathrm{~N}^{2}(\varphi) \cos ^{2} \varphi
\end{array}\right]
$$

## A. 4 Geocentric Metric - Latitude ( $\psi$ ), Longitude ( $\lambda$ )

The equation of the surface that uses latitude and longitude as both central angles of the ellipsoid would be as follows:

Eq 66.
Ellipsoid:

$$
\frac{X^{2}+Y^{2}}{a^{2}}+\frac{Z^{2}}{b^{2}}=1
$$

Using classical mathematical trigonometry, the above equations can be expressed, using geocentric latitude $\varphi_{c}$ and longitude $\lambda$. Taking the equations $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ expressed functions in geocentric or geodetic coordinates, $(\varphi, \lambda)$. This is essentially the create the radius of curvature along the $\varphi$ (meridians) and $\lambda$ (parallels) coordinate lines. The metric uses the squares of the radii of curvature.
Geocentric ellipsoidal coordinates, $S^{2}(\psi, \lambda) \subset \mathbb{E}^{3}(X, Y, Z)$ where:

Eq 67. Geocentric:

$$
\left.\begin{array}{rl}
\vec{X}=\left[\begin{array}{c}
a \cos \psi \cos \lambda \\
a \cos \psi \sin \lambda \\
b \sin \psi
\end{array}\right] \\
\mathrm{J}\left(\frac{X, Y, Z}{\varphi, \lambda}\right) & =\left[\frac{\partial \vec{X}}{\partial \psi}=d \psi \quad \frac{\partial \vec{X}}{\partial \lambda}=d \lambda\right.
\end{array}\right] \quad \begin{array}{cc} 
\\
& =\left[\frac{\partial}{\partial \psi}\left[\begin{array}{c}
a \cos \psi \sin \lambda \\
a \cos \psi \cos \lambda \\
b \sin \psi
\end{array}\right] \quad \frac{\partial}{\partial \lambda}\left[\begin{array}{c}
a \cos \psi \sin \lambda \\
a \cos \psi \cos \lambda \\
b \sin \psi
\end{array}\right]\right] \\
& =\left[\begin{array}{cc}
-a \sin \psi \sin \lambda & a \cos \psi \cos \lambda \\
-a \sin \psi \cos \lambda & -a \cos \psi \sin \lambda \\
b \cos \psi & 0
\end{array}\right]
\end{array}
$$

Eq 69. $\vec{u}_{1}=\frac{\partial \vec{X}}{\partial \psi}=[-a \sin \psi \cos \lambda,-a \sin \psi \sin \lambda, b \cos \psi]$

Eq 70. $\quad \vec{u}_{2}=\frac{\partial \vec{X}}{\partial \lambda}=[-a \cos \psi \sin \lambda, a \cos \psi \cos \lambda, 0]$

Eq 71.

$$
\vec{u}_{1} \bullet \vec{u}_{1}=E=a_{11}=a^{2} \sin ^{2} \psi+b^{2} \cos ^{2} \psi
$$

$$
\begin{aligned}
& \vec{u}_{1} \bullet \vec{u}_{2}=F=a_{12}=a_{21}=0 \\
& \vec{u}_{2} \bullet \vec{u}_{2}=G=a_{22}=a^{2} \cos ^{2} \psi
\end{aligned}
$$

## A. 5 First Fundamental Form Using Geocentric Latitude " $\Psi$ ":

Eq 72. Geocentric Metric $\quad\left[a_{i j}\right]=\left[\begin{array}{cc}E & F \\ F & G\end{array}\right]=\left[\begin{array}{cc}a^{2} \sin ^{2} \psi+b^{2} \cos ^{2} \psi & 0 \\ 0 & a^{2} \cos ^{2} \psi\end{array}\right]$

This creates the pieces for the first fundamental form, which is a vector inner product for $\vec{u}$ and $\vec{v}$ in the vector space for the coordinates $(\psi, \lambda)$ whose vectors spanned by $(\vec{v}, \vec{u})$ as defined above. In other words, these are vectors for the coordinate space of $(\psi, \lambda)$ i.e. the reference ellipsoid. The inner product $\left[g_{i j}\right]$ also implies that any vectors in the $\psi$-direction at a point is always perpendicular to vectors in the $\lambda$-direction.

## A. 6 Geocentric Metric on a sphere - Latitude ( $\psi$ ), Longitude ( $\boldsymbol{\lambda}$ )

If $a=b$ then the ellipsoid is a sphere ( $a=r=b$ ) and the first fundamental of the sphere using geocentric latitude " $\psi$ " and longitude " $\lambda$ " is:

Eq 73. Geocentric Metric on a spherer:

$$
\left[\begin{array}{ll}
E & F \\
F & G
\end{array}\right]=\left[a_{i j}\right]=\left[\begin{array}{cc}
r^{2} & 0 \\
0 & r^{2} \cos \psi
\end{array}\right]
$$

On the sphere, the geocentric " $\psi$ " and geodetic " $\varphi$ " latitude are the same because the circle's eccentricity in 0 . It should be remembered that for a sphere, $\mathrm{r}=\mathrm{a}=\mathrm{b}$, and any metric will work. For example, the next equation can be used to calculate this by doing just that:

Eq 74.

$$
\sin ^{2} \psi+\cos ^{2} \psi=1
$$

Geocentric measures are measured along a line from the center of the ellipsoid (origin of the coordinate system) to the point. Geodetic latitude makes things a bit more complex. A geocentric latitude is the slope of the upward normal from the surface of the ellipsoid which is equal to the geocentric latitude at the equator and the poles.

In all cases, the integral for length of a curve in equation (70) and the area or a region W in equations in (74) are valid for each fundamental form for the variables (in these cases "latitude", " $\psi$ " or " $\varphi$ ", and longitude " $\lambda$ ") used in the calculation of the form.

## A. $7 \quad$ Three-Dimensional Geodetic Metric $(\varphi, \lambda, h)$

This clause shows that the standard mapping between geodetic $(\varphi, \lambda)$ and ECEF (X,Y, Z) are consistent.

Eq 75. $\quad \mathrm{X}$ in geodetic:

$$
X=(N(\varphi)+h) \cos \varphi \cos \lambda
$$

Eq 76. Yingeodetic:

$$
Y=(N(\varphi)+h) \cos \varphi \sin \lambda
$$

$$
Z=\left(N(\varphi)\left(1-e^{2}\right)+h\right) \sin \varphi
$$

Eq 78. $\quad$ Radius of parallel: $\rho=\sqrt{X^{2}+Y^{2}}=\sqrt{(N(\varphi)+h)^{2} \cos ^{2} \varphi}=(N(\varphi)+h) \cos \varphi$

Eq 79. Coordinates:

$$
\begin{aligned}
X & =\rho \cos \lambda=(N(\varphi)+h) \cos \varphi \cos \lambda, \\
Y & =\rho \sin \lambda=(N(\varphi)+h) \cos \varphi \sin \lambda \\
Z & =\left(N(\varphi)\left(1-e^{2}\right)+h\right) \sin \varphi
\end{aligned}
$$

Using classical mathematical trigonometry, the above equations can be expressed, using geodetic latitude $\varphi$ and longitude $\lambda$. Taking the equations $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ expressed functions in geocentric coordinates, $(\varphi, \lambda)$. This is essentially the creation of the Jacobian of the coordinate transformation between ECEF $(\mathrm{X}, \mathrm{Y}, \mathrm{Z})$ and latitude - longitude $(\varphi, \lambda)$.

Eq 80.

$$
N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \quad N^{\prime}(\varphi)=\frac{a e^{2} \sin \varphi \cos \varphi}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}
$$

Eq 81.

$$
\left[\begin{array}{l}
X \\
Y \\
Z
\end{array}\right]=\left[\begin{array}{l}
(N(\varphi)+h) \cos \varphi \cos \lambda \\
(N(\varphi)+h) \cos \varphi \sin \lambda \\
(N(\varphi)+h)\left(1-e^{2}\right) \sin \varphi
\end{array}\right]
$$

This creates the components for the first fundamental form, which is a vector inner product for $\vec{u}$ and $\vec{v}$ in the vector space for the coordinates $(\varphi, \lambda)$ whose vectors spanned by $(\overrightarrow{\boldsymbol{v}}, \overrightarrow{\boldsymbol{u}})$ as defined above. In other words, these are vectors for the coordinate space of $(\varphi, \lambda)$ i.e. the reference ellipsoid. The inner product also implies that any vectors in the $\varphi$-direction at a point is always perpendicular to vectors in the $\lambda$-direction.
Geocentric measures are measured along a line from the center of the ellipsoid (origin of the coordinate system) to the point. Geodetic latitude makes things a bit more complex. A geocentric latitude is slope of the upward normal from the surface of the ellipsoid which is equal to the geocentric latitude at the equator and the poles.

Similar calculations for geodetic latitude are a bit more complicated. The equations for this form has been, often with slightly different variable names, around for quite a long time, See Bomford [3] (at least in the $3^{\text {rd }}$ and later editions), Burkholder [4], Hotine [16], IOGP[19], Jekeli [20], , Ligas [22], Panigrahi [26], Torge [31], Clynch [6], [7] and [8]. The differences in the various versions of the model were essentially in the choice of variable names, and the details on the calculations.

The first step in each case is to determine the local perpendicular and the length of the this principal normal as a function of latitude $\mathrm{N}(\varphi)$, with respect to the east-west "longitude lines".

Eq 82. $\quad J\left(\frac{X, Y, Z}{\varphi, \lambda, h}\right)=\left[\frac{\partial \vec{X}}{\partial \varphi}=d \varphi \quad \frac{\partial \vec{X}}{\partial \lambda}=d \lambda \quad \frac{\partial \vec{X}}{\partial h}=d h\right]$

Eq 83. $\quad J\left(\frac{X, Y, Z}{\varphi, \lambda, h}\right)=\left[\begin{array}{l}\vec{u}_{1}=d \varphi=\frac{\partial}{\partial \varphi}\left[\begin{array}{l}(N(\varphi)+h) \cos \varphi \cos \lambda \\ (N(\varphi)+h) \cos \varphi \sin \lambda \\ (N(\varphi)+h)\left(1-e^{2}\right) \sin \varphi\end{array}\right] \\ \vec{u}_{2}=d \lambda=\frac{\partial}{\partial \lambda}\left[\begin{array}{l}(N(\varphi)+h) \cos \varphi \cos \lambda \\ (N(\varphi)+h) \cos \varphi \sin \lambda \\ (N(\varphi)+h)\left(1-e^{2}\right) \sin \varphi\end{array}\right] \\ \vec{u}_{3}=d h=\frac{\partial}{\partial h}\left[\begin{array}{l}(N(\varphi)+h) \cos \varphi \cos \lambda \\ (N(\varphi)+h) \cos \varphi \sin \lambda \\ (N(\varphi)+h)\left(1-e^{2}\right) \sin \varphi\end{array}\right]\end{array}\right]$
Eq 84. $\quad\left[\begin{array}{ll}d \varphi & d \lambda \\ d\end{array}\right]=\left[\begin{array}{c}{\left[\begin{array}{c}N^{\prime}(\varphi) \cos \varphi \cos \lambda-(N(\varphi)+h) \sin \varphi \cos \lambda \\ N^{\prime}(\varphi) \cos \varphi \sin \lambda-(N(\varphi)+h) \sin \varphi \sin \lambda \\ N^{\prime}(\varphi)\left(1-e^{2}\right) \sin \varphi+(N(\varphi)+h)\left(1-e^{2}\right) \cos \varphi\end{array}\right]} \\ {\left[\begin{array}{c}-(N(\varphi)+h) \cos \varphi \sin \lambda \\ (N(\varphi)+h) \cos \varphi \cos \lambda \\ 0\end{array}\right]} \\ {\left[\begin{array}{c}\cos \varphi \cos \lambda \\ \cos \varphi \sin \lambda \\ \left(1-e^{2}\right) \sin \varphi\end{array}\right]}\end{array}\right]$
Eq 85. $\quad \vec{u}_{1}=\frac{\partial \vec{X}}{\partial \varphi}=\left[\begin{array}{l}\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-(N(\varphi)+h) \sin \varphi\right) \cos \lambda \\ \left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-(N(\varphi)+h) \sin \varphi\right) \sin \lambda \\ \left(1-e^{2}\right)\left(\mathrm{N}^{\prime}(\varphi) \sin \varphi+(N(\varphi)+h) \cos \varphi\right)\end{array}\right]$

Eq 86. $\quad \vec{u}_{2}=\frac{\partial \vec{X}}{\partial \lambda}=\left[\begin{array}{c}-(N(\varphi)+h) \cos \varphi \sin \lambda \\ (N(\varphi)+h) \cos \varphi \cos \lambda \\ 0\end{array}\right]$
Eq 87. $\quad \vec{u}_{3}=\frac{\partial \vec{X}}{\partial h}=\left[\begin{array}{c}\cos \varphi \cos \lambda \\ \cos \varphi \sin \lambda \\ \left(1-e^{2}\right) \sin \varphi\end{array}\right]$

First fundamental form for geodetic coordinates $(\varphi, \lambda)$ :

$$
\begin{aligned}
& a_{1,1}=\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi-(\mathrm{N}(\varphi)+h) \sin \varphi\right)^{2}+\left(1-e^{2}\right)^{2}\left(\mathrm{~N}^{\prime}(\varphi) \sin \varphi+(\mathrm{N}(\varphi)+h) \cos \varphi\right)^{2}=m^{2}(\varphi) \\
& a_{2,2}=(\mathrm{N}(\varphi))^{2} \cos ^{2} \varphi\left(\sin ^{2} \lambda+\cos ^{2} \lambda\right)=\mathrm{N}^{2}(\varphi) \cos ^{2} \varphi=(\mathrm{N}(\varphi) \cos \varphi)^{2}=\rho^{2}(\varphi)
\end{aligned}
$$

Eq 88.

$$
\begin{aligned}
& a_{3,3}=\cos ^{2} \varphi+\frac{b^{4}}{a^{4}} \sin ^{2} \varphi=\cos ^{2} \varphi+\left(1-e^{2}\right)^{2} \sin ^{2} \varphi \\
& a_{i, j}=\vec{u}_{i} \cdot \vec{u}_{j}=0 \text { iff } i \neq j
\end{aligned}
$$

$$
\left[a_{i, j}\right]=
$$

Eq 89. $\left[\begin{array}{ccc}\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi+\mathrm{N}(\varphi) \sin \varphi\right)^{2}+\frac{b^{4}}{a^{4}}(\mathrm{~N}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi)^{2} & 0 & 0 \\ 0 & \mathrm{~N}^{2}(\varphi) \cos ^{2} \varphi & 0 \\ 0 & 0 & \cos ^{2} \varphi+\frac{b^{4}}{a^{4}} \sin ^{2} \varphi\end{array}\right]$

## Annex B Metric Integrals and Numeric Approximations

## B. 1 Length and Area Integrals.

This section defines the Riemannian metrics, which are integrals derived from Gauss's work and Newton's calculus. In these cases, the calculus is rather difficult and usually does not lead to simple integrations in closed form. This means there are not simple formulas as in the Pythagorean metric. This means that the best viable solutions are numeric integrations which are approximations based on the simple summations that show-up in the basic definitions of an integral an area under a curve.

This is quite easy to understand, an integral $\int_{a}^{b} f(t) d t$ is the area under the curve $f(t)$ between the axis and the curve between $t=a$ and $t=b$. These solutions in fairly simple loops that reiterate summations that approximate this area. The key to getting a good approximation is to use longer and longer summations based on smaller and smaller intervals for latitude and longitude e.g. shorter $\Delta \varphi$ 's and $\Delta \lambda$ 's (see below).
For geodetic coordinates, the following metric functions apply:

$$
E^{2}(\varphi)=\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi+\mathrm{N}(\varphi) \sin \varphi\right)^{2}+\frac{b^{4}}{a^{4}}\left(\mathrm{~N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right)^{2}
$$

Eq 90. Meridian radius: $\quad=M^{2}(\varphi)$

$$
M(\rho)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{3 / 2}}=\sqrt{E(\varphi)}
$$

Eq 91. Parallel radius:

$$
\begin{aligned}
& \mathrm{G}(\varphi)=\mathrm{N}(\varphi)^{2} \cos ^{2} \varphi=\rho^{2}(\varphi)=(N(\varphi) \cos \varphi)^{2} \\
& \rho(\varphi)=N(\varphi) \cos \varphi=\sqrt{G(\varphi)}
\end{aligned}
$$

The relationship between $E(\varphi)=m^{2}(\varphi)$ is addressed in Annex B.2. A formal proof is yet to be found, but extensive numeric testing indicates $E(\varphi)=\mathrm{m}^{2}(\varphi)$ are equal for all values of " $\varphi$ ". The most common set of parameters are from WGS84:

## B. 2 The Curve Length Integral and the Numeric Alternative

Integration in calculus is inherently difficult, because unlike derivatives, there is often not a fixed procedure. In the use of the integrals in the above narrative are a line integral to calculate the length of a geometry (curve) ( $\mathrm{E}, \mathrm{F}$ and G are distances in meters, and $\varphi$ and $\lambda$ are angles represented in radians, i.e. no unit (radians are a ratio and inherently unitless, e.g. $\pi=180^{\circ}, 1^{\circ}=\pi / 180=0.0174532925199$ ). In all cases in this paper $\varphi$ and $\lambda$ lines are orthogonal everywhere, so $\mathrm{F} \equiv 0$.
To understand what follows, we need to understand the relationship between $\varphi, \lambda$, and t on a curve c : $c(t)=(\varphi(t), \lambda(t))$; we have 3 sequences for $\left(\varphi_{i}, \lambda_{i}, t_{i}\right)$ where $c\left(t_{i}\right)=\left(\varphi\left(t_{i}\right), \lambda\left(t_{i}\right)\right)=\left(\varphi_{i}, \lambda_{i}\right)$. Assuming
the $\Delta \varphi$, and $\Delta \lambda$, are small enough to keep the radii of curvatures within a small area so that they are "fairly smooth".

Eq 92. Curve $=\left[\begin{array}{c}\mathrm{c}(\mathrm{t})=\left\{\mathrm{c}\left(\mathrm{t}_{i}\right)=\left(\varphi_{i}, \lambda_{i}\right) \mid i=0,1,2,3 \ldots n ;\right\} \\ \Delta \varphi_{i}=\left|\varphi_{i}-\varphi_{i-1}\right| ; \Delta \lambda_{i}=\left|\lambda_{i}-\lambda_{i-1}\right|\end{array}\right]$

Eq 93. Length Integral:

$$
L_{c}=\int_{a}^{b} \sqrt{E(\varphi)\left(\frac{d \varphi}{d t}\right)^{2}+G(\varphi)\left(\frac{d \lambda}{d t}\right)^{2}} d t
$$

$$
L_{c}=\lim _{\substack{n \rightarrow \infty \\ \Delta \rightarrow 0}} \sum_{i=1}^{n} \sqrt{E\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\left(\Delta \varphi_{i}\right)^{2}+G\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\left(\Delta \lambda_{i}\right)^{2}}
$$

$$
=\lim _{\substack{n \rightarrow \infty \\ \Delta \rightarrow 0}} \sum_{i=1}^{n} \sqrt{M^{2}\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\left(\Delta \varphi_{i}\right)^{2}+\rho^{2}\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\left(\Delta \lambda_{i}\right)^{2}}
$$

As seen above, as the $\Delta \varphi$ and $\Delta \lambda$ grow smaller and more numerous, the numeric calculations use the Pythagorean formula which works best if the square bounded by $\Delta \varphi_{i}$, and $\Delta \lambda_{i}$ is on the order of a fraction of degree for both for both latitude and longitude. This works because in small areas the classical geometry works in what we refer to as engineering diagrams or plans. In this approximation we used the midpoint value for $E$ and $G$ between $\varphi_{i}$ and $\varphi_{i-1}$. In the examples in
Each of the possible options do something equivalent, approximating the area of the polygon or trapezoid under the function in the integral by multiplying the width of the represented by the values of $\Delta \varphi$ and $\Delta \lambda$, where the function functions $E$ and $G$ in that supply the "meters per radian" for the locality of the arc.
Annex B also contains the mechanism for these integrals to be calculated using summations. This derives directly from the definition of an integral as the limit of longer and longer sums.
The idea is to divide the subdivisions into smaller and smaller ones, for example, by placing a new value for " $s$ " between each existing pair, doubling the number of intervals and halving each interval by inserting a midpoint.

Eq 94. Curve in $(\varphi, \lambda)$

$$
\begin{aligned}
a & =t_{0}, t_{1}, \ldots, t_{n}=b \\
\Delta t_{i} & =t_{i}-t_{i-1} \\
\left(\varphi_{i}, \lambda_{i}\right) & =\left(\varphi\left(t_{i}\right), \lambda\left(t_{i}\right)\right)
\end{aligned}
$$

$$
\begin{aligned}
\Delta \varphi_{i} & =\varphi_{i}-\varphi_{i-1} \\
\Delta \lambda_{i} & =\lambda_{i}-\lambda_{i-1} \\
t_{i} & =t_{2 i}^{\prime} \text { and } t_{2 i+1}^{\prime}=\frac{t_{i}+t_{i+1}}{2}=\frac{t_{2 i}^{\prime}+t_{2 i+2}^{\prime}}{2}
\end{aligned}
$$

Eq 95.

$$
\begin{aligned}
\Delta L_{i} & =\left(\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right)^{2} \Delta \varphi_{i}^{2}+\left(\frac{\rho\left(\lambda_{i}\right)+\rho\left(\lambda_{i-1}\right)}{2}\right)^{2} \Delta \lambda_{i}^{2}\right)^{\frac{1}{2}} \\
L_{c} & =\lim _{n \rightarrow \infty}\left(\sum_{i=1}^{n} \Delta L_{i}\right)
\end{aligned}
$$

$$
\begin{aligned}
\Delta A_{c} & =\left(\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right) \Delta \varphi_{i} \times\left(\frac{\rho\left(\lambda_{i}\right)+\rho\left(\lambda_{i-1}\right)}{2}\right) \Delta \lambda_{i}\right) \\
A_{c} & =\lim _{n \rightarrow \infty}\left(\sum_{i=1}^{n} \Delta A_{c i}\right)
\end{aligned}
$$

Each this iterative summation will get closer to the actual $L_{c}$ if sufficiently accurate number formats are used (64-bit double-precision at the least). The usual approach might be using the number of nodes used in the digital curve (as defined in ISO 19107 Geographic information - Spatial schema, and half each interval length (doubling the count) each time until subsequent difference in subsequent iterations are within the desired error budget.

## B. 3 The Surface Area Integral

The surface area integral calculates the area of a subsurface of the reference surface (ellipsoid), which is simple product of the length times the width in $\sqrt{\boldsymbol{E}(\boldsymbol{\varphi}) \boldsymbol{G}(\boldsymbol{\varphi})} \boldsymbol{\Delta} \boldsymbol{\varphi} \Delta \lambda$. Note that in both cases $(\sqrt{\boldsymbol{E}(\boldsymbol{\varphi})} \Delta \varphi$ and $\sqrt{\boldsymbol{G}(\boldsymbol{\varphi})} \Delta \lambda$ ) gives you the number of meters in a width in $\Delta \varphi$ direction and a length in $\Delta \lambda$ direction respectively. The two delta-angles are in radians, and the $E$ and $G$ parts just change angles to meters.

So, in a way the Riemannian measures of length and area depend on the usual Euclidean measures, good as long as the values of $\Delta \varphi$ or $\Delta \lambda$ are sufficiently small for the purpose. In a truly echo of history, what we are doing is exactly that which the $3^{\text {rd }}$ century BC Greeks were using to approximate $\pi$ by creating polygons to closely approximate the length or surface of the spheroid or circle. The area integral for the geodetic fundamental forms in this paper the area integral is (recall that $\mathrm{F}=0$ ).

Eq 96. Area integral

$$
\begin{aligned}
A_{S} & =\iint_{W} \sqrt{E(\varphi) G(\varphi)} d \varphi d \lambda=\iint_{W} \sqrt{E(\varphi)} \sqrt{G(\varphi)} d \varphi d \lambda \\
\sqrt{E(\varphi)} & =M(\varphi)=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2} \\
\sqrt{G(\varphi)} & =N(\varphi) \mid \cos \varphi
\end{aligned}
$$

The summation approximations for this integral break the area into square using subsets of the $\varphi$ and $\lambda$ squares. So, if the latitude is between $\varphi_{0}, \ldots \varphi_{\mathrm{n}}$, and $\lambda_{0}, \ldots \lambda_{\mathrm{n}}$ :
The difference between the line integral and the area integral is the dimension of the summation sections. There are alternatives to what is below, but the same idea may be used with various methods of getting to smaller and smaller polygons.

1. Start with the minimum bounding rectangle. It is a square box that contains the entire area.
2. Slice all polygons into smaller polygons; any way that works, rectangles and triangles seem to work best. Throw out any that do not overlap the area $\boldsymbol{A}$.
3. For each remaining polygon measure the area in degrees in latitude and longitude. This is actually a unitless area, the units come from the integrand (the function between the long $S$ " $\int$ " and the variable differentials " $\mathrm{d} \varphi \mathrm{d} \lambda$ ", which is in square meters (which is the way the derivations were made above, $\sqrt{E(\varphi)}$, and $\sqrt{G(\varphi)}$ are meters, so EG is therefore square meters).
4. Take the centroid each of the polygons (easy on squares and triangles); call it "p", and calculate an integrand at " p " inside the polygon preferably near the center, e.g. $\sqrt{E(p) G(p)}$ and multiply it by the "radian area" of the " $\mathrm{d} \varphi \mathrm{d} \lambda$ " polygon, e.g. $\sqrt{E(p) G(p)} \Delta \varphi \Delta \lambda=m(\varphi) \rho(\varphi) \Delta \varphi \Delta \lambda$ if it is the original still the original angular rectangle.
5. Sum all of these and keep it as the approximate area (recall, it is a number of square meters).
6. If the last 2 answers were very close within each other of the intended accuracy limit, stop and report the area at the integral value
7. If you did not stop at the last step, return step 2 and repeat.

## B. 4 The Integrals and their Numeric Approximations

Eq 97. The length integral:

$$
L_{c}=\int_{a}^{b} \sqrt{E(\varphi)\left(\frac{d \varphi}{d t}\right)^{2}+G(\varphi)\left(\frac{d \lambda}{d t}\right)^{2}} d t
$$

The idea is that the curve in question is written as a function of " $t$ " (think of time moving onward). So, our curve " $c$ " is a function of " $t$ " which keeps track or latitude, $\varphi$ and longitude $\lambda$, so we write:

Eq 98. Derivtive of curve: $\left[c\left(t_{i}\right)=\left(\varphi\left(t_{i}\right), \lambda\left(t_{i}\right)\right)\right] \Rightarrow\left[\frac{d c}{d t}=\frac{d}{d t} c\left(t_{i}\right)=\left(\frac{d}{d t} \varphi\left(t_{i}\right), \frac{d}{d t} \lambda\left(t_{i}\right)\right)\right]$

Which basically says that the derivative of a curve is the tangent vector (in physics, it is the velocity vector). Therefore, using the equation, the function (for velocity) it the square root of the functions from the first fundament form and an approximation of the vectors. In the geometry specification (ISO 19107) defines curves as a sequence of points: $\left\{\overrightarrow{\boldsymbol{p}}_{\boldsymbol{i}}=\left(\boldsymbol{\varphi}_{\boldsymbol{i}}, \boldsymbol{\lambda}_{\boldsymbol{i}}\right) \mid \boldsymbol{i}=\mathbf{0} ., \boldsymbol{n}\right\}$ and \{interpolation='curve type' $\}$ such that the curve between $\overrightarrow{\boldsymbol{p}}_{\boldsymbol{i - 1}}$ and $\overrightarrow{\boldsymbol{p}}_{\boldsymbol{i}}$ :

Eq 99. Generic curve

$$
\begin{aligned}
& c\left(t_{i}\right)=\left(\varphi_{i}, \lambda_{i}\right), \mathrm{i}=0,1,2, \ldots, \mathrm{n} \\
& \Delta \varphi_{i}=\varphi_{i}-\varphi_{i-1} ; \\
& \Delta \lambda_{i}=\lambda_{i}-\lambda_{i-1} \text { and } \frac{d \varphi}{d t} \cong \frac{\Delta \varphi_{i}}{\Delta \mathrm{t}_{i}} \text { and } \frac{d \lambda}{d t} \cong \frac{\Delta \lambda_{i}}{\Delta \mathrm{t}_{i}}
\end{aligned}
$$

Eq 100. Length of curve:

$$
\begin{gathered}
{\left[\frac{d \varphi}{d t} \cong \frac{\Delta \varphi_{i}}{\Delta \mathrm{t}_{i}} \text { and } \frac{d \lambda}{d t} \cong \frac{\Delta \lambda_{i}}{\Delta \mathrm{t}_{i}}\right] \Rightarrow} \\
L_{c}=\int_{a}^{b} \sqrt{E(\varphi)\left(\frac{d \varphi}{d t}\right)^{2}+G(\varphi)\left(\frac{d \lambda}{d t}\right)^{2}} d t \cong \\
\lim _{\substack{\Delta t \rightarrow 0 \\
n \rightarrow \infty}}\left(\sum_{i=0}^{n}\left(\left(M\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\right) \Delta \varphi_{i}^{2}+\left(\rho\left(\frac{\varphi_{i}+\varphi_{i-1}}{2}\right)\right) \Delta \lambda_{i}^{2}\right)^{1 / 2}\right)
\end{gathered}
$$

In general, both $\varphi$ and $\lambda$ will most often both vary simultaneously. In some of the examples below for lines of latitude or lines of longitude, allows a simplified length integral ( $\boldsymbol{L}_{\boldsymbol{c}}$ ), by using deltas for either longitude or latitude, but not both. Which changes the square root of the sum of squares, to a single $E$ or $G$ summation term.

It should be noted that both $E(\varphi)$ and $G(\varphi)$ are always only a function of latitude and always positive (always a sum of squares). In the $L_{c}$ integrals, the $\Delta \varphi$ and $\Delta \lambda$ are squared and then square-rooted, meaning they are also always contributing positively in the numeric integration for the line-length integrals.

Eq 101. N-S Distance

$$
L_{c}(\varphi)=\int_{a}^{b} \sqrt{E(\varphi)} d \varphi=\lim _{\substack{\Delta t \rightarrow 0 \\ n \rightarrow \infty}}\left(\sum_{i=0}^{n}\left(\frac{\sqrt{E\left(\varphi_{i}\right)}+\sqrt{E\left(\varphi_{i-1}\right)}}{2}\left|\Delta \varphi_{i}\right|\right)\right)
$$

$$
=\int_{a}^{b} M(\varphi) d \varphi=\lim _{\substack{\Delta t \rightarrow 0 \\ n \rightarrow \infty}}\left(\sum_{i=0}^{n}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\left|\Delta \varphi_{i}\right|\right)\right)
$$

$$
\Delta \varphi_{i}=\varphi_{i}-\varphi_{i-1}
$$

$$
\begin{aligned}
L_{c}(\lambda) & =\int_{a}^{b} \sqrt{G(\varphi)} d \lambda=\lim _{\substack{\Delta t \rightarrow 0 \\
n \rightarrow \infty}}\left(\sum_{i=0}^{n}\left(\frac{\sqrt{G\left(\varphi_{i}\right)}+\sqrt{G\left(\varphi_{i-1}\right)}}{2}\left|\Delta \lambda_{i}\right|\right)\right) \\
& =\int_{a}^{b} \rho(\varphi) d \lambda=\lim _{\substack{\Delta t \rightarrow 0 \\
n \rightarrow \infty}}\left(\sum_{i=0}^{n}\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2}\left|\Delta \lambda_{i}\right|\right)\right) ; \\
\Delta \lambda_{i} & =\lambda_{i}-\lambda_{i-1}
\end{aligned}
$$

It is the case that these two functions are equivalent to local square of the radius of curvature or lines of varying latitude lines (meridians) for $\sqrt{E(\varphi)}=M(\varphi)=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2}$ and for lines of varying longitude (parallels) for $\sqrt{G(\varphi)}$ for $\rho(\varphi)=N(\varphi)|\cos \varphi|$.

## Annex C Examples

The two tables below describe the length of the meridians (north-south lines) and parallels (east-west) in terms of $\Delta \varphi$ and $\Delta \lambda$ converted to meters based on the radius of curvature of these curves on the ellipsoid. With this information and the integrals in Annex B. What they show is that using $\Delta \varphi$ and $\Delta \lambda$ of approximately a degree or less, local distances, and thereby local areas, can be calculated down to the level of centimeter accuracy.

## C. 1 Length of a Degree of Longitude

The table below uses the equations in Annex B to calculate the length of a degree of longitude along parallels of the various latitudes, partially repeated below the table. This table would be north-south symmetric, so that the value for " $\varphi$ " is the same as " $-\varphi$ ", The given the radius "r" derives from the computation below the table, circumference is " $2 \pi r$ ". The formula below is valid for any $\varphi$ in radians ( $2 \pi$ radians $=360^{\circ}$ ). The radius " $\rho$ " falls out of the calculations in equation below. The radius of curvature in meters at latitude " $\varphi$ " in the plane of the parallel of latitude.

Eq 103. Parallel radius $\quad \rho(\varphi)=\sqrt{X^{2}+Y^{2}}=\frac{a \cos \varphi}{\sqrt{1-e^{2} \sin ^{2} \varphi}}=N(\varphi) \cos \varphi$

A full circle is $360^{\circ}$ degrees, and $2 \pi$ radians. The radius of a circle of latitude is $\rho(\varphi)$ and so the circumference of the circle of parallel is $2 \pi \rho(\varphi)$. Table 1 show the radius at each latitude (the equator radius is the semimajor axis " $a=6,378,137$ meters" which is 111.319 km per degree, and $6,378,137$ meters per radian)" to the pole where the radius is "0.0". Bomford [3] calls $\rho(\varphi)$ the radius of the parallel of latitude. The local circumference at latitude " $\varphi$ " is " $c(\varphi)=2 \pi \rho(\varphi)$ ". This table did not require any integral but is directly observed by analysis of the ellipsoid, see equation (80). Clynch [9] also deals with the value of the radius function " $\rho(\varphi)$ ". Unlike latitude the length of $\Delta \lambda$ along a parallel is constant on any ellipsoid. In each row below the length of the parallel is calculated from the latitude, where the radius of the circular parallel.

Table 1. Length of Parallel of Longitude at each quarter Latitude:

| Latitude in Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | Km in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 0.000000000 | 6,378,137.000000 | 40,075.016686 | 0.000000000 | 111.31949079 |
| 0.25 | 0.004363323 | 6,378,076.691178 | 40,074.637754 | 0.378931504 | 111.31843821 |
| 0.50 | 0.008726646 | 6,377,895.765791 | 40,073.50966 | 1.136787733 | 111.31528046 |
| 0.75 | 0.013089969 | 6,377,594.227076 | 40,071.606343 | 1.894623623 | 111.31001762 |
| 1.00 | 0.017453293 | 6,377,172.080428 | 40,068.953917 | 2.652425615 | 111.30264977 |
| 1.25 | 0.021816616 | 6,376,629.333401 | 40,065.543737 | 3.410180150 | 111.29317705 |
| 1.50 | 0.026179939 | 6,375,965.995704 | 40,061.375863 | 4.167873669 | 111.28159962 |
| 1.75 | 0.030543262 | 6,375,182.079207 | 40,056.450371 | 4.925492616 | 111.26791770 |
| 2.00 | 0.034906585 | 6,374,277.597936 | 40,050.767347 | 5.683023432 | 111.25213152 |
| 2.25 | 0.039269908 | 6,373,252.568076 | 40,044.326895 | 6.440452561 | 111.23424137 |
| 2.50 | 0.043633231 | 6,372,107.007966 | 40,037.129128 | 7.197766447 | 111.21424800 |
| 2.75 | 0.047996554 | 6,370,840.938107 | 40,029.174177 | 7.954951535 | 111.19215049 |
| 3.00 | 0.052359878 | 6,369,454.381155 | 40,020.462182 | 8.711994272 | 111.16795051 |
| 3.25 | 0.056723201 | 6,367,947.361922 | 40,010.993301 | 9.468881105 | 111.14164806 |
| 3.50 | 0.061086524 | 6,366,319.907377 | 40,000.767703 | 10.22559848 | 111.11324362 |
| 3.75 | 0.065449847 | 6,364,572.046647 | 39,989.785570 | 10.98213286 | 111.08273769 |
| 4.00 | 0.06981317 | 6,362,703.811015 | 39,978.047099 | 11.73847068 | 111.05013083 |
| 4.25 | 0.074176493 | 6,360,715.233918 | 39,965.552501 | 12.49459840 | 111.01542361 |
| 4.50 | 0.078539816 | 6,358,606.350952 | 39,952.301998 | 13.2550247 | 110.97861666 |
| 4.75 | 0.082903139 | 6,356,377.199865 | 39,938.295829 | 14.00616936 | 110.93971064 |
| 5.00 | 0.087266463 | 6,354,027.820562 | 39,923.534244 | 14.76158551 | 110.89870623 |
| 5.25 | 0.091629786 | 6,351,558.255103 | 39,908.017506 | 15.51673740 | 110.85560418 |
| 5.50 | 0.095993109 | 6,348,968.547703 | 39,891.745895 | 16.27161149 | 110.81040526 |
| 5.75 | 0.100356432 | 6,346,258.744728 | 39,874.719700 | 17.02619423 | 110.76311028 |
| 6.00 | 0.104719755 | 6,343,428.894702 | 39,856.939228 | 17.78047211 | 110.71372008 |
| 6.25 | 0.109083078 | 6,340,479.048298 | 39,838.404797 | 18.53443158 | 110.66223555 |
| 6.50 | 0.113446401 | 6,337,409.258345 | 39,819.116738 | 19.28805913 | 110.60865760 |
| 6.75 | 0.117809725 | 6,334,219.579823 | 39,799.075396 | 20.04134122 | 110.55298721 |
| 7.00 | 0.122173048 | 6,330,910.069865 | 39,778.281132 | 20.79426434 | 110.49522537 |
| 7.25 | 0.126536371 | 6,327,480.787754 | 39,756.734317 | 21.54681497 | 110.43537310 |
| 7.50 | 0.130899694 | 6,323,931.794925 | 39,734.435337 | 22.29897960 | 110.37343149 |
| 7.75 | 0.135263017 | 6,320,263.154963 | 39,711.384593 | 23.05074471 | 110.30940165 |
| 8.00 | 0.13962634 | 6,316,474.933602 | 39,687.582496 | 23.80209679 | 110.24328471 |
| 8.25 | 0.143989663 | 6,312,567.198729 | 39,663.029474 | 24.55302234 | 110.17508187 |
| 8.50 | 0.148352986 | 6,308,540.020374 | 39,637.725966 | 25.30350786 | 110.10479435 |
| 8.75 | 0.152716310 | 6,304,393.470721 | 39,611.672426 | 26.05353986 | 110.03242341 |
| 9.00 | 0.157079633 | 6,300,127.624097 | 39,584.869321 | 26.80310483 | 109.95797034 |
| 9.25 | 0.161442956 | 6,295,742.556979 | 39,557.317132 | 27.55218929 | 109.88143648 |
| 9.50 | 0.165806279 | 6,291,238.347988 | 39,529.016352 | 28.30077975 | 109.80282320 |


| Latitude in Degrees | Latitude in Radians | Radius in Meters $\qquad$ of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | Km in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 9.75 | 0.170169602 | 6,286,615.077892 | 39,499.967489 | 29.04886274 | 109.72213191 |
| 10.00 | 0.174532925 | 6,281,872.829603 | 39,470.171065 | 29.79642477 | 109.63936407 |
| 10.25 | 0.178896248 | 6,277,011.688179 | 39,439.627612 | 30.54345238 | 109.55452114 |
| 10.50 | 0.183259571 | 6,272,031.740818 | 39,408.337680 | 31.28993209 | 109.46760467 |
| 10.75 | 0.187622895 | 6,266,933.076864 | 39,376.301830 | 32.03585044 | 109.37861619 |
| 11.00 | 0.191986218 | 6,261,715.787801 | 39,343.520636 | 32.78119398 | 109.28755732 |
| 11.25 | 0.196349541 | 6,256,379.967255 | 39,309.994686 | 33.52594926 | 109.19442968 |
| 11.50 | 0.200712864 | 6,250,925.710992 | 39,275.724584 | 34.27010282 | 109.09923495 |
| 11.75 | 0.205076187 | 6,245,353.116916 | 39,240.710942 | 35.01364122 | 109.00197484 |
| 12.00 | 0.209439510 | 6,239,662.285072 | 39,204.954391 | 35.75655103 | 108.90265109 |
| 12.25 | 0.213802833 | 6,233,853.317642 | 39,168.455573 | 36.49881881 | 108.80126548 |
| 12.50 | 0.218166156 | 6,227,926.318942 | 39,131.215141 | 37.24043114 | 108.69781984 |
| 12.75 | 0.222529480 | 6,221,881.395428 | 39,093.233767 | 37.98137461 | 108.59231602 |
| 13.00 | 0.226892803 | 6,215,718.655689 | 39,054.512131 | 38.72163578 | 108.48475592 |
| 13.25 | 0.231256126 | 6,209,438.210446 | 39,015.050930 | 39.46120127 | 108.37514147 |
| 13.50 | 0.235619449 | 6,203,040.172557 | 38,974.850872 | 40.20005766 | 108.26347464 |
| 13.75 | 0.239982772 | 6,196,524.657008 | 38,933.912680 | 40.93819157 | 108.14975745 |
| 14.00 | 0.244346095 | 6,189,891.780918 | 38,892.237091 | 41.67558959 | 108.03399192 |
| 14.25 | 0.248709418 | 6,183,141.663535 | 38,849.824853 | 42.41223836 | 107.91618015 |
| 14.50 | 0.253072742 | 6,176,274.426237 | 38,806.676728 | 43.14812449 | 107.79632424 |
| 14.75 | 0.257436065 | 6,169,290.192528 | 38,762.793493 | 43.88323462 | 107.67442637 |
| 15.00 | 0.261799388 | 6,162,189.088038 | 38,718.175938 | 44.61755539 | 107.55048872 |
| 15.25 | 0.266162711 | 6,154,971.240525 | 38,672.824865 | 45.35107344 | 107.42451351 |
| 15.50 | 0.270526034 | 6,147,636.779869 | 38,626.741089 | 46.08377543 | 107.29650303 |
| 15.75 | 0.274889357 | 6,140,185.838073 | 38,579.925441 | 46.81564802 | 107.16645956 |
| 16.00 | 0.279252680 | 6,132,618.549263 | 38,532.378763 | 47.54667787 | 107.03438545 |
| 16.25 | 0.283616003 | 6,124,935.049683 | 38,484.101912 | 48.27685166 | 106.90028309 |
| 16.50 | 0.287979327 | 6,117,135.477700 | 38,435.095756 | 49.00615609 | 106.76415488 |
| 16.75 | 0.292342650 | 6,109,219.973795 | 38,385.361178 | 49.73457783 | 106.62600327 |
| 17.00 | 0.296705973 | 6,101,188.680568 | 38,334.899074 | 50.46210360 | 106.48583076 |
| 17.25 | 0.301069296 | 6,093,041.742734 | 38,283.710354 | 51.18872010 | 106.34363987 |
| 17.50 | 0.305432619 | 6,084,779.307120 | 38,231.795940 | 51.91441405 | 106.19943317 |
| 17.75 | 0.309795942 | 6,076,401.522668 | 38,179.156768 | 52.63917218 | 106.05321324 |
| 18.00 | 0.314159265 | 6,067,908.540429 | 38,125.793787 | 53.36298122 | 105.90498274 |
| 18.25 | 0.318522588 | 6,059,300.513566 | 38,071.707959 | 54.08582791 | 105.75474433 |
| 18.50 | 0.322885912 | 6,050,577.597346 | 38,016.900260 | 54.80769902 | 105.60250072 |
| 18.75 | 0.327249235 | 6,041,739.949148 | 37,961.371678 | 55.52858131 | 105.44825466 |
| 19.00 | 0.331612558 | 6,032,787.728451 | 37,905.123217 | 56.24846155 | 105.29200894 |
| 19.25 | 0.335975881 | 6,023,721.096841 | 37,848.155890 | 56.96732652 | 105.13376636 |
| 19.50 | 0.340339204 | 6,014,540.218004 | 37,790.470727 | 57.68516302 | 104.97352980 |


| Latitude <br> in <br> Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | $K m$ in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 19.75 | 0.344702527 | 6,005,245.257727 | 37,732.068769 | 58.40195784 | 104.81130214 |
| 20.00 | 0.349065850 | 5,995,836.383896 | 37,672.951072 | 59.11769781 | 104.64708631 |
| 20.25 | 0.353429174 | 5,986,313.766495 | 37,613.118702 | 59.83236974 | 104.48088528 |
| 20.50 | 0.357792497 | 5,976,677.577600 | 37,552.572741 | 60.54596048 | 104.31270206 |
| 20.75 | 0.362155820 | 5,966,927.991385 | 37,491.314284 | 61.25845686 | 104.14253968 |
| 21.00 | 0.366519143 | 5,957,065.184112 | 37,429.344439 | 61.96984574 | 103.97040122 |
| 21.25 | 0.370882466 | 5,947,089.334135 | 37,366.664325 | 62.68011400 | 103.79628979 |
| 21.50 | 0.375245789 | 5,937,000.621898 | 37,303.275076 | 63.38924850 | 103.62020855 |
| 21.75 | 0.379609112 | 5,926,799.229927 | 37,239.177840 | 64.09723614 | 103.44216067 |
| 22.00 | 0.383972435 | 5,916,485.342837 | 37,174.373776 | 64.80406382 | 103.26214938 |
| 22.25 | 0.388335759 | 5,906,059.147324 | 37,108.864058 | 65.50971846 | 103.08017794 |
| 22.50 | 0.392699082 | 5,895,520.832164 | 37,042.649871 | 66.21418697 | 102.89624964 |
| 22.75 | 0.397062405 | 5,884,870.588214 | 36,975.732415 | 66.91745631 | 102.71036782 |
| 23.00 | 0.401425728 | 5,874,108.608405 | 36,908.112901 | 67.61951341 | 102.52253584 |
| 23.25 | 0.405789051 | 5,863,235.087746 | 36,839.792556 | 68.32034524 | 102.33275710 |
| 23.50 | 0.410152374 | 5,852,250.223317 | 36,770.772617 | 69.01993878 | 102.14103505 |
| 23.75 | 0.414515697 | 5,841,154.214269 | 36,701.054336 | 69.71828102 | 101.94737316 |
| 24.00 | 0.418879020 | 5,829,947.261822 | 36,630.638977 | 70.41535895 | 101.75177494 |
| 24.25 | 0.423242344 | 5,818,629.569262 | 36,559.527818 | 71.11115960 | 101.55424394 |
| 24.50 | 0.427605667 | 5,807,201.341941 | 36,487.722148 | 71.80566999 | 101.35478374 |
| 24.75 | 0.431968990 | 5,795,662.787271 | 36,415.223270 | 72.49887717 | 101.15339797 |
| 25.00 | 0.436332313 | 5,784,014.114726 | 36,342.032502 | 73.19076819 | 100.95009028 |
| 25.25 | 0.440695636 | 5,772,255.535836 | 36,268.151172 | 73.88133012 | 100.74486437 |
| 25.50 | 0.445058959 | 5,760,387.264187 | 36,193.580622 | 74.57055004 | 100.53772395 |
| 25.75 | 0.449422282 | 5,748,409.515419 | 36,118.322207 | 75.25841507 | 100.32867280 |
| 26.00 | 0.453785606 | 5,736,322.507223 | 36,042.377295 | 75.94491231 | 100.11771471 |
| 26.25 | 0.458148929 | 5,724,126.459335 | 35,965.747266 | 76.63002889 | 99.90485352 |
| 26.50 | 0.462512252 | 5,711,821.593542 | 35,888.433514 | 77.31375196 | 99.69009309 |
| 26.75 | 0.466875575 | 5,699,408.133671 | 35,810.437445 | 77.99606868 | 99.47343735 |
| 27.00 | 0.471238898 | 5,686,886.305590 | 35,731.760479 | 78.67696622 | 99.25489022 |
| 27.25 | 0.475602221 | 5,674,256.337207 | 35,652.404047 | 79.35643177 | 99.03445569 |
| 27.50 | 0.479965544 | 5,661,518.458466 | 35,572.369595 | 80.03445255 | 98.81213776 |
| 27.75 | 0.484328867 | 5,648,672.901344 | 35,491.658579 | 80.71101577 | 98.58794050 |
| 28.00 | 0.488692191 | 5,635,719.899847 | 35,410.272470 | 81.38610869 | 98.36186797 |
| 28.25 | 0.493055514 | 5,622,659.690012 | 35,328.212752 | 82.05971855 | 98.13392431 |
| 28.50 | 0.497418837 | 5,609,492.509899 | 35,245.480919 | 82.73183262 | 97.90411366 |
| 28.75 | 0.501782160 | 5,596,218.599591 | 35,162.078481 | 83.40243821 | 97.67244022 |
| 29.00 | 0.506145483 | 5,582,838.201193 | 35,078.006958 | 84.07152262 | 97.43890822 |
| 29.25 | 0.510508806 | 5,569,351.558823 | 34,993.267885 | 84.73907318 | 97.20352190 |
| 29.50 | 0.514872129 | 5,555,758.918618 | 34,907.862808 | 85.40507722 | 96.96628558 |


| Latitude <br> in <br> Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | $K m$ in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 29.75 | 0.519235452 | 5,542,060.528723 | 34,821.793286 | 86.06952212 | 96.72720357 |
| 30.00 | 0.523598776 | 5,528,256.639293 | 34,735.060890 | 86.73239525 | 96.48628025 |
| 30.25 | 0.527962099 | 5,514,347.502487 | 34,647.667206 | 87.39368402 | 96.24352002 |
| 30.50 | 0.532325422 | 5,500,333.372467 | 34,559.613830 | 88.05337583 | 95.99892731 |
| 30.75 | 0.536688745 | 5,486,214.505397 | 34,470.902372 | 88.71145813 | 95.75250659 |
| 31.00 | 0.541052068 | 5,471,991.159433 | 34,381.534454 | 89.36791838 | 95.50426237 |
| 31.25 | 0.545415391 | 5,457,663.594727 | 34,291.511710 | 90.02274404 | 95.25419919 |
| 31.50 | 0.549778714 | 5,443,232.073422 | 34,200.835787 | 90.67592263 | 95.00232163 |
| 31.75 | 0.554142038 | 5,428,696.859646 | 34,109.508346 | 91.32744164 | 94.74863429 |
| 32.00 | 0.558505361 | 5,414,058.219511 | 34,017.531057 | 91.97728861 | 94.49314183 |
| 32.25 | 0.562868684 | 5,399,316.421111 | 33,924.905606 | 92.62545111 | 94.23584891 |
| 32.50 | 0.567232007 | 5,384,471.734515 | 33,831.633689 | 93.27191671 | 93.97676025 |
| 32.75 | 0.571595330 | 5,369,524.431769 | 33,737.717016 | 93.91667300 | 93.71588060 |
| 33.00 | 0.575958653 | 5,354,474.786886 | 33,643.157309 | 94.55970761 | 93.45321475 |
| 33.25 | 0.580321976 | 5,339,323.075848 | 33,547.956300 | 95.20100817 | 93.18876750 |
| 33.50 | 0.584685299 | 5,324,069.576601 | 33,452.115738 | 95.84056235 | 92.92254372 |
| 33.75 | 0.589048623 | 5,308,714.569050 | 33,355.637380 | 96.47835783 | 92.65454828 |
| 34.00 | 0.593411946 | 5,293,258.335058 | 33,258.522998 | 97.11438232 | 92.38478611 |
| 34.25 | 0.597775269 | 5,277,701.158440 | 33,160.774374 | 97.74862355 | 92.11326215 |
| 34.50 | 0.602138592 | 5,262,043.324960 | 33,062.393305 | 98.38106926 | 91.83998140 |
| 34.75 | 0.606501915 | 5,246,285.122330 | 32,963.381598 | 99.01170724 | 91.56494888 |
| 35.00 | 0.610865238 | 5,230,426.840200 | 32,863.741073 | 99.64052527 | 91.28816965 |
| 35.25 | 0.615228561 | 5,214,468.770164 | 32,763.473561 | 100.2675112 | 91.00964878 |
| 35.50 | 0.619591884 | 5,198,411.205744 | 32,662.580909 | 100.8926528 | 90.72939141 |
| 35.75 | 0.623955208 | 5,182,254.442399 | 32,561.064971 | 101.5159381 | 90.44740270 |
| 36.00 | 0.628318531 | 5,165,998.777511 | 32,458.927616 | 102.1373548 | 90.16368782 |
| 36.25 | 0.632681854 | 5,149,644.510385 | 32,356.170725 | 102.7568909 | 89.87825201 |
| 36.50 | 0.637045177 | 5,133,191.942247 | 32,252.796190 | 103.3745344 | 89.59110053 |
| 36.75 | 0.641408500 | 5,116,641.376236 | 32,148.805917 | 103.9902732 | 89.30223866 |
| 37.00 | 0.645771823 | 5,099,993.117404 | 32,044.201822 | 104.6040953 | 89.01167173 |
| 37.25 | 0.650135146 | 5,083,247.472708 | 31,938.985833 | 105.2159887 | 88.71940509 |
| 37.50 | 0.654498469 | 5,066,404.751009 | 31,833.159892 | 105.8259415 | 88.42544414 |
| 37.75 | 0.658861793 | 5,049,465.263064 | 31,726.725950 | 106.4339418 | 88.12979431 |
| 38.00 | 0.663225116 | 5,032,429.321529 | 31,619.685972 | 107.0399775 | 87.83246103 |
| 38.25 | 0.667588439 | 5,015,297.240946 | 31,512.041935 | 107.6440370 | 87.53344982 |
| 38.50 | 0.671951762 | 4,998,069.337744 | 31,403.795827 | 108.2461083 | 87.23276619 |
| 38.75 | 0.676315085 | 4,980,745.930233 | 31,294.949648 | 108.8461795 | 86.93041569 |
| 39.00 | 0.680678408 | 4,963,327.338603 | 31,185.505409 | 109.4442309 | 86.62640391 |
| 39.25 | 0.685041731 | 4,945,813.884912 | 31,075.465134 | 110.0402749 | 86.32073648 |
| 39.50 | 0.689405055 | 4,928,205.893089 | 30,964.830858 | 110.6342755 | 86.01341905 |


| Latitude <br> in <br> Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | $K m$ in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 39.75 | 0.693768378 | 4,910,503.688925 | 30,853.604629 | 111.2262291 | 85.70445730 |
| 40.00 | 0.698131701 | 4,892,707.600073 | 30,741.788505 | 111.8161240 | 85.39385696 |
| 40.25 | 0.702495024 | 4,874,817.956036 | 30,629.384557 | 112.4039486 | 85.08162377 |
| 40.50 | 0.706858347 | 4,856,835.088170 | 30,516.394865 | 112.9896912 | 84.76776351 |
| 40.75 | 0.711221670 | 4,838,759.329674 | 30,402.821525 | 113.5733402 | 84.45228201 |
| 41.00 | 0.715584993 | 4,820,591.015588 | 30,288.666641 | 114.1548841 | 84.13518511 |
| 41.25 | 0.719948316 | 4,802,330.482789 | 30,173.932330 | 114.7343114 | 83.81647869 |
| 41.50 | 0.724311640 | 4,783,978.069981 | 30,058.620719 | 115.3116105 | 83.49616866 |
| 41.75 | 0.728674963 | 4,765,534.117696 | 29,942.733949 | 115.8867700 | 83.17426097 |
| 42.00 | 0.733038286 | 4,746,998.968287 | 29,826.274171 | 116.4597784 | 82.85076159 |
| 42.25 | 0.737401609 | 4,728,372.965922 | 29,709.243546 | 117.0306244 | 82.52567652 |
| 42.50 | 0.741764932 | 4,709,656.456578 | 29,591.644250 | 117.5992965 | 82.19901181 |
| 42.75 | 0.746128255 | 4,690,849.788040 | 29,473.478466 | 118.1657834 | 81.87077352 |
| 43.00 | 0.750491578 | 4,671,953.309892 | 29,354.748393 | 118.7300739 | 81.54096776 |
| 43.25 | 0.754854901 | 4,652,967.373514 | 29,235.456236 | 119.2921565 | 81.20960066 |
| 43.50 | 0.759218225 | 4,633,892.332076 | 29,115.604216 | 119.8520201 | 80.87667838 |
| 43.75 | 0.763581548 | 4,614,728.540531 | 28,995.194562 | 120.4096535 | 80.54220712 |
| 44.00 | 0.767944871 | 4,595,476.355612 | 28,874.229517 | 120.9650454 | 80.20619310 |
| 44.25 | 0.772308194 | 4,576,136.135828 | 28,752.711332 | 121.5181848 | 79.86864259 |
| 44.50 | 0.776671517 | 4,556,708.241454 | 28,630.642272 | 122.0690605 | 79.52956187 |
| 44.75 | 0.781034840 | 4,537,193.034529 | 28,508.024610 | 122.6176614 | 79.18895725 |
| 45.00 | 0.785398163 | 4,517,590.878849 | 28,384.860634 | 123.1639766 | 78.84683509 |
| 45.25 | 0.789761487 | 4,497,902.139962 | 28,261.152639 | 123.7079949 | 78.50320177 |
| 45.50 | 0.794124810 | 4,478,127.185163 | 28,136.902934 | 124.2497054 | 78.15806370 |
| 45.75 | 0.798488133 | 4,458,266.383487 | 28,012.113836 | 124.7890973 | 77.81142732 |
| 46.00 | 0.802851456 | 4,438,320.105703 | 27,886.787677 | 125.3261595 | 77.46329910 |
| 46.25 | 0.807214779 | 4,418,288.724311 | 27,760.926795 | 125.8608812 | 77.11368554 |
| 46.50 | 0.811578102 | 4,398,172.613532 | 27,634.533544 | 126.3932517 | 76.76259318 |
| 46.75 | 0.815941425 | 4,377,972.149305 | 27,507.610284 | 126.9232600 | 76.41002857 |
| 47.00 | 0.820304748 | 4,357,687.709282 | 27,380.159388 | 127.4508955 | 76.05599830 |
| 47.25 | 0.824668072 | 4,337,319.672818 | 27,252.183241 | 127.9761474 | 75.70050900 |
| 47.50 | 0.829031395 | 4,316,868.420969 | 27,123.684236 | 128.4990051 | 75.34356732 |
| 47.75 | 0.833394718 | 4,296,334.336484 | 26,994.664778 | 129.0194579 | 74.98517994 |
| 48.00 | 0.837758041 | 4,275,717.803798 | 26,865.127282 | 129.5374953 | 74.62535356 |
| 48.25 | 0.842121364 | 4,255,019.209028 | 26,735.074176 | 130.0531065 | 74.26409493 |
| 48.50 | 0.846484687 | 4,234,238.939967 | 26,604.507895 | 130.5662812 | 73.90141082 |
| 48.75 | 0.85084801 | 4,213,377.386073 | 26,473.430886 | 131.0770089 | 73.53730802 |
| 49.00 | 0.855211333 | 4,192,434.938469 | 26,341.845607 | 131.5852791 | 73.17179335 |
| 49.25 | 0.859574657 | 4,171,411.989933 | 26,209.754525 | 132.0910814 | 72.80487368 |
| 49.50 | 0.86393798 | 4,150,308.934891 | 26,077.160120 | 132.5944054 | 72.43655589 |


| Latitude in Degrees | Latitude in Radians | Radius in Meters $\qquad$ of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | Km in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 49.75 | 0.868301303 | 4,129,126.169414 | 25,944.064879 | 133.0952408 | 72.06684689 |
| 50.00 | 0.872664626 | 4,107,864.091207 | 25,810.471302 | 133.5935774 | 71.69575362 |
| 50.25 | 0.877027949 | 4,086,523.099606 | 25,676.381897 | 134.0894049 | 71.32328305 |
| 50.50 | 0.881391272 | 4,065,103.595569 | 25,541.799184 | 134.5827131 | 70.94944218 |
| 50.75 | 0.885754595 | 4,043,605.981672 | 25,406.725692 | 135.0734918 | 70.57423803 |
| 51.00 | 0.890117919 | 4,022,030.662098 | 25,271.163961 | 135.5617309 | 70.19767767 |
| 51.25 | 0.894481242 | 4,000,378.042635 | 25,135.116541 | 136.0474205 | 69.81976817 |
| 51.50 | 0.898844565 | 3,978,648.530665 | 24,998.585990 | 136.5305503 | 69.44051664 |
| 51.75 | 0.903207888 | 3,956,842.535161 | 24,861.574880 | 137.0111106 | 69.05993022 |
| 52.00 | 0.907571211 | 3,934,960.466675 | 24,724.085789 | 137.4890912 | 68.67801608 |
| 52.25 | 0.911934534 | 3,913,002.737339 | 24,586.121306 | 137.9644823 | 68.29478141 |
| 52.50 | 0.916297857 | 3,890,969.760847 | 24,447.684032 | 138.4372742 | 67.91023342 |
| 52.75 | 0.920661180 | 3,868,861.952457 | 24,308.776575 | 138.9074568 | 67.52437938 |
| 53.00 | 0.925024504 | 3,846,679.728981 | 24,169.401555 | 139.3750206 | 67.13722654 |
| 53.25 | 0.929387827 | 3,824,423.508777 | 24,029.561599 | 139.8399558 | 66.74878222 |
| 53.50 | 0.933751150 | 3,802,093.711742 | 23,889.259346 | 140.3022526 | 66.35905374 |
| 53.75 | 0.938114473 | 3,779,690.759303 | 23,748.497445 | 140.7619016 | 65.96804846 |
| 54.00 | 0.942477796 | 3,757,215.074415 | 23,607.278551 | 141.2188931 | 65.57577375 |
| 54.25 | 0.946841119 | 3,734,667.081548 | 23,465.605334 | 141.6732175 | 65.18223704 |
| 54.50 | 0.951204442 | 3,712,047.206682 | 23,323.480469 | 142.1248654 | 64.78744575 |
| 54.75 | 0.955567765 | 3,689,355.877298 | 23,180.906641 | 142.5738274 | 64.39140734 |
| 55.00 | 0.959931089 | 3,666,593.522374 | 23,037.886547 | 143.0200940 | 63.99412930 |
| 55.25 | 0.964294412 | 3,643,760.572373 | 22,894.422891 | 143.4636560 | 63.59561914 |
| 55.50 | 0.968657735 | 3,620,857.459237 | 22,750.518387 | 143.9045039 | 63.19588441 |
| 55.75 | 0.973021058 | 3,597,884.616380 | 22,606.175759 | 144.3426287 | 62.79493266 |
| 56.00 | 0.977384381 | 3,574,842.478680 | 22,461.397738 | 144.7780210 | 62.39277149 |
| 56.25 | 0.981747704 | 3,551,731.482471 | 22,316.187066 | 145.2106718 | 61.98940852 |
| 56.50 | 0.986111027 | 3,528,552.065534 | 22,170.546494 | 145.6405719 | 61.58485137 |
| 56.75 | 0.990474351 | 3,505,304.667091 | 22,024.478781 | 146.0677123 | 61.17910773 |
| 57.00 | 0.994837674 | 3,481,989.727795 | 21,877.986697 | 146.4920840 | 60.77218527 |
| 57.25 | 0.999200997 | 3,458,607.689725 | 21,731.073019 | 146.9136781 | 60.36409172 |
| 57.50 | 1.003564320 | 3,435,158.996373 | 21,583.740534 | 147.3324855 | 59.95483482 |
| 57.75 | 1.007927643 | 3,411,644.092642 | 21,435.992036 | 147.7484976 | 59.54442232 |
| 58.00 | 1.012290966 | 3,388,063.424832 | 21,287.830331 | 148.1617055 | 59.13286203 |
| 58.25 | 1.016654289 | 3,364,417.440635 | 21,139.258230 | 148.5721005 | 58.72016175 |
| 58.50 | 1.021017612 | 3,340,706.589127 | 20,990.278556 | 148.9796738 | 58.30632932 |
| 58.75 | 1.025380936 | 3,316,931.320758 | 20,840.894140 | 149.3844169 | 57.89137261 |
| 59.00 | 1.029744259 | 3,293,092.087345 | 20,691.107818 | 149.7863211 | 57.47529950 |
| 59.25 | 1.034107582 | 3,269,189.342061 | 20,540.922440 | 150.1853780 | 57.05811789 |
| 59.50 | 1.038470905 | 3,245,223.539431 | 20,390.340861 | 150.5815790 | 56.63983573 |


| Latitude in Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | Km in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 59.75 | 1.042834228 | 3,221,195.135320 | 20,239.365946 | 150.9749157 | 56.22046096 |
| 60.00 | 1.047197551 | 3,197,104.586924 | 20,088.00566 | 151.3653797 | 55.80000157 |
| 60.25 | 1.051560874 | 3,172,952.352764 | 19,936.247603 | 151.7529628 | 55.37846556 |
| 60.50 | 1.055924197 | 3,148,738.892675 | 19,784.109947 | 152.1376567 | 54.95586096 |
| 60.75 | 1.060287521 | 3,124,464.667800 | 19,631.590494 | 152.5194531 | 54.53219582 |
| 61.00 | 1.064650844 | 3,100,130.140577 | 19,478.692150 | 152.8983439 | 54.10747819 |
| 61.25 | 1.069014167 | 3,075,735.774734 | 19,325.417829 | 153.2743210 | 53.68171619 |
| 61.50 | 1.073377490 | 3,051,282.035278 | 19,171.770452 | 153.6473765 | 53.25491792 |
| 61.75 | 1.077740813 | 3,026,769.388488 | 19,017.752950 | 154.0175021 | 52.82709153 |
| 62.00 | 1.082104136 | 3,002,198.301904 | 18,863.368260 | 154.3846902 | 52.39824517 |
| 62.25 | 1.086467459 | 2,977,569.244319 | 18,708.619327 | 154.7489328 | 51.96838702 |
| 62.50 | 1.090830782 | 2,952,882.685768 | 18,553.509105 | 155.1102220 | 51.53752529 |
| 62.75 | 1.095194106 | 2,928,139.097524 | 18,398.040555 | 155.4685501 | 51.10566821 |
| 63.00 | 1.099557429 | 2,903,338.952081 | 18,242.216645 | 155.8239095 | 50.67282402 |
| 63.25 | 1.103920752 | 2,878,482.723153 | 18,086.040353 | 156.1762924 | 50.23900098 |
| 63.50 | 1.108284075 | 2,853,570.885660 | 17,929.514662 | 156.5256913 | 49.80420739 |
| 63.75 | 1.112647398 | 2,828,603.915717 | 17,772.642563 | 156.8720987 | 49.36845156 |
| 64.00 | 1.117010721 | 2,803,582.290630 | 17,615.427056 | 157.2155071 | 48.93174182 |
| 64.25 | 1.121374044 | 2,778,506.488883 | 17,457.871147 | 157.5559091 | 48.49408652 |
| 64.50 | 1.125737368 | 2,753,376.990129 | 17,299.977850 | 157.8932973 | 48.05549403 |
| 64.75 | 1.130100691 | 2,728,194.275181 | 17,141.750185 | 158.2276646 | 47.61597274 |
| 65.00 | 1.134464014 | 2,702,958.826003 | 16,983.191181 | 158.5590035 | 47.17553106 |
| 65.25 | 1.138827337 | 2,677,671.125698 | 16,824.303874 | 158.8873070 | 46.73417743 |
| 65.50 | 1.143190660 | 2,652,331.658502 | 16,665.091306 | 159.2125680 | 46.29192030 |
| 65.75 | 1.147553983 | 2,626,940.909770 | 16,505.556527 | 159.5347794 | 45.84876813 |
| 66.00 | 1.151917306 | 2,601,499.365971 | 16,345.702593 | 159.8539342 | 45.40472942 |
| 66.25 | 1.156280629 | 2,576,007.514674 | 16,185.532567 | 160.1700255 | 44.95981269 |
| 66.50 | 1.160643953 | 2,550,465.844542 | 16,025.049521 | 160.4830465 | 44.51402645 |
| 66.75 | 1.165007276 | 2,524,874.845319 | 15,864.256531 | 160.7929903 | 44.06737925 |
| 67.00 | 1.169370599 | 2,499,235.007819 | 15,703.156680 | 161.0998503 | 43.61987967 |
| 67.25 | 1.173733922 | 2,473,546.823924 | 15,541.753061 | 161.4036196 | 43.17153628 |
| 67.50 | 1.178097245 | 2,447,810.786562 | 15,380.048769 | 161.7042918 | 42.72235769 |
| 67.75 | 1.182460568 | 2,422,027.389707 | 15,218.046909 | 162.0018603 | 42.27235252 |
| 68.00 | 1.186823891 | 2,396,197.128365 | 15,055.750590 | 162.2963185 | 41.82152942 |
| 68.25 | 1.191187214 | 2,370,320.498563 | 14,893.162930 | 162.5876602 | 41.36989703 |
| 68.50 | 1.195550538 | 2,344,397.997340 | 14,730.287051 | 162.8758788 | 40.91746403 |
| 68.75 | 1.199913861 | 2,318,430.122737 | 14,567.126083 | 163.1609682 | 40.46423912 |
| 69.00 | 1.204277184 | 2,292,417.373786 | 14,403.683161 | 163.4429220 | 40.01023100 |
| 69.25 | 1.208640507 | 2,266,360.25502 | 14,239.961427 | 163.7217342 | 39.55544841 |
| 69.50 | 1.213003830 | 2,240,259.253868 | 14,075.964028 | 163.9973986 | 39.09990008 |


| Latitude <br> in <br> Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | $K m$ in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 69.75 | 1.217367153 | 2,214,114.885828 | 13,911.694119 | 164.2699091 | 38.64359478 |
| 70.00 | 1.221730476 | 2,187,927.649279 | 13,747.154859 | 164.5392599 | 38.18654128 |
| 70.25 | 1.226093800 | 2,161,698.048054 | 13,582.349414 | 164.8054450 | 37.72874837 |
| 70.50 | 1.230457123 | 2,135,426.586917 | 13,417.280955 | 165.0684586 | 37.27022488 |
| 70.75 | 1.234820446 | 2,109,113.771550 | 13,251.952661 | 165.3282949 | 36.81097961 |
| 71.00 | 1.239183769 | 2,082,760.108543 | 13,086.367712 | 165.5849482 | 36.35102142 |
| 71.25 | 1.243547092 | 2,056,366.105383 | 12,920.529300 | 165.8384129 | 35.89035917 |
| 71.50 | 1.247910415 | 2,029,932.270445 | 12,754.440616 | 166.0886833 | 35.42900171 |
| 71.75 | 1.252273738 | 2,003,459.112979 | 12,588.104862 | 166.3357540 | 34.96695795 |
| 72.00 | 1.256637061 | 1,976,947.143101 | 12,421.525243 | 166.5796196 | 34.50423678 |
| 72.25 | 1.261000385 | 1,950,396.871779 | 12,254.704968 | 166.8202747 | 34.04084713 |
| 72.50 | 1.265363708 | 1,923,808.810830 | 12,087.647254 | 167.0577139 | 33.57679793 |
| 72.75 | 1.269727031 | 1,897,183.472899 | 11,920.355322 | 167.2919321 | 33.11209812 |
| 73.00 | 1.274090354 | 1,870,521.371456 | 11,752.832398 | 167.5229240 | 32.64675666 |
| 73.25 | 1.278453677 | 1,843,823.020780 | 11,585.081713 | 167.7506847 | 32.18078254 |
| 73.50 | 1.282817000 | 1,817,088.935952 | 11,417.106504 | 167.9752090 | 31.71418473 |
| 73.75 | 1.287180323 | 1,790,319.632843 | 11,248.910012 | 168.1964920 | 31.24697226 |
| 74.00 | 1.291543646 | 1,763,515.628099 | 11,080.495483 | 168.4145288 | 30.77915412 |
| 74.25 | 1.295906970 | 1,736,677.439137 | 10,911.866169 | 168.6293146 | 30.31073936 |
| 74.50 | 1.300270293 | 1,709,805.584127 | 10,743.025324 | 168.8408446 | 29.84173701 |
| 74.75 | 1.304633616 | 1,682,900.581986 | 10,573.976210 | 169.0491141 | 29.37215614 |
| 75.00 | 1.308996939 | 1,655,962.952365 | 10,404.722092 | 169.2541186 | 28.90200581 |
| 75.25 | 1.313360262 | 1,628,993.215636 | 10,235.266238 | 169.4558536 | 28.43129511 |
| 75.50 | 1.317723585 | 1,601,991.892885 | 10,065.611924 | 169.6543144 | 27.96003312 |
| 75.75 | 1.322086908 | 1,574,959.505896 | 9,895.762427 | 169.8494967 | 27.48822896 |
| 76.00 | 1.326450232 | 1,547,896.577144 | 9,725.721031 | 170.0413963 | 27.01589175 |
| 76.25 | 1.330813555 | 1,520,803.629781 | 9,555.491022 | 170.2300088 | 26.54303062 |
| 76.50 | 1.335176878 | 1,493,681.187625 | 9,385.075692 | 170.4153301 | 26.06965470 |
| 76.75 | 1.339540201 | 1,466,529.775149 | 9,214.478336 | 170.5973559 | 25.59577315 |
| 77.00 | 1.343903524 | 1,439,349.917470 | 9,043.702253 | 170.7760824 | 25.12139515 |
| 77.25 | 1.348266847 | 1,412,142.140339 | 8,872.750748 | 170.9515055 | 24.64652986 |
| 77.50 | 1.352630170 | 1,384,906.970125 | 8,701.627127 | 171.1236213 | 24.17118646 |
| 77.75 | 1.356993493 | 1,357,644.933808 | 8,530.334700 | 171.2924260 | 23.69537417 |
| 78.00 | 1.361356817 | 1,330,356.558966 | 8,358.876785 | 171.4579159 | 23.21910218 |
| 78.25 | 1.365720140 | 1,303,042.373763 | 8,187.256697 | 171.6200871 | 22.74237972 |
| 78.50 | 1.370083463 | 1,275,702.906938 | 8,015.477761 | 171.7789363 | 22.26521600 |
| 78.75 | 1.374446786 | 1,248,338.687793 | 7,843.543302 | 171.9344597 | 21.78762028 |
| 79.00 | 1.378810109 | 1,220,950.246182 | 7,671.456648 | 172.0866539 | 21.30960180 |
| 79.25 | 1.383173432 | 1,193,538.112498 | 7,499.221132 | 172.2355156 | 20.83116981 |
| 79.50 | 1.387536755 | 1,166,102.817665 | 7,326.840091 | 172.3810414 | 20.35233359 |


| Latitude <br> in <br> Degrees | Latitude in Radians | Radius in Meters of Parallel $\rho(\varphi)$ | Circumferen ce in Km | Difference of Parallels in Km | $K m$ in a $\lambda$ Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 79.75 | 1.391900078 | 1,138,644.893121 | 7,154.316863 | 172.5232281 | 19.87310240 |
| 80.00 | 1.396263402 | 1,111,164.870810 | 6,981.654790 | 172.6620724 | 19.39348553 |
| 80.25 | 1.400626725 | 1,083,663.283170 | 6,808.857219 | 172.7975714 | 18.91349227 |
| 80.50 | 1.404990048 | 1,056,140.663121 | 6,635.927497 | 172.9297219 | 18.43313194 |
| 80.75 | 1.409353371 | 1,028,597.544051 | 6,462.868976 | 173.0585211 | 17.95241382 |
| 81.00 | 1.413716694 | 1,001,034.459806 | 6,289.685010 | 173.1839659 | 17.47134725 |
| 81.25 | 1.418080017 | 973,451.944681 | 6,116.378956 | 173.3060538 | 16.98994154 |
| 81.50 | 1.422443340 | 945,850.533404 | 5,942.954174 | 173.4247818 | 16.50820604 |
| 81.75 | 1.426806664 | 918,230.761124 | 5,769.414027 | 173.5401474 | 16.02615007 |
| 82.00 | 1.431169987 | 890,593.163403 | 5,595.761879 | 173.6521479 | 15.54378300 |
| 82.25 | 1.435533310 | 862,938.276200 | 5,422.001098 | 173.7607809 | 15.06111416 |
| 82.50 | 1.439896633 | 835,266.635864 | 5,248.135054 | 173.8660440 | 14.57815293 |
| 82.75 | 1.444259956 | 807,578.779115 | 5,074.167119 | 173.9679347 | 14.09490866 |
| 83.00 | 1.448623279 | 779,875.243040 | 4,900.100668 | 174.0664508 | 13.61139075 |
| 83.25 | 1.452986602 | 752,156.565074 | 4,725.939078 | 174.1615901 | 13.12760855 |
| 83.50 | 1.457349925 | 724,423.282993 | 4,551.685728 | 174.2533505 | 12.64357147 |
| 83.75 | 1.461713249 | 696,675.934900 | 4,377.343998 | 174.3417298 | 12.15928888 |
| 84.00 | 1.466076572 | 668,915.059213 | 4,202.917272 | 174.4267262 | 11.67477020 |
| 84.25 | 1.470439895 | 641,141.194654 | 4,028.408934 | 174.5083377 | 11.19002482 |
| 84.50 | 1.474803218 | 613,354.880236 | 3,853.822372 | 174.5865625 | 10.70506214 |
| 84.75 | 1.479166541 | 585,556.655249 | 3,679.160973 | 174.6613988 | 10.21989159 |
| 85.00 | 1.483529864 | 557,747.059254 | 3,504.428128 | 174.7328450 | 9.73452258 |
| 85.25 | 1.487893187 | 529,926.632063 | 3,329.627228 | 174.8008994 | 9.24896452 |
| 85.50 | 1.492256510 | 502,095.913735 | 3,154.761668 | 174.8655605 | 8.76322686 |
| 85.75 | 1.496619834 | 474,255.444558 | 2,979.834841 | 174.9268269 | 8.27731900 |
| 86.00 | 1.50983157 | 446,405.765037 | 2,804.850144 | 174.9846972 | 7.79125040 |
| 86.25 | 1.505346480 | 418,547.415888 | 2,629.810974 | 175.0391701 | 7.30503048 |
| 86.50 | 1.509709803 | 390,680.938017 | 2,454.720730 | 175.0902443 | 6.81866869 |
| 86.75 | 1.514073126 | 362,806.872517 | 2,279.582811 | 175.1379188 | 6.33217447 |
| 87.00 | 1.518436449 | 334,925.760648 | 2,104.400618 | 175.1821924 | 5.84555727 |
| 87.25 | 1.522799772 | 307,038.143829 | 1,929.177554 | 175.2230642 | 5.35882654 |
| 87.50 | 1.527163095 | 279,144.563626 | 1,753.917021 | 175.2605333 | 4.87199172 |
| 87.75 | 1.531526419 | 251,245.561738 | 1,578.622422 | 175.2945987 | 4.38506228 |
| 88.00 | 1.535889742 | 223,341.679987 | 1,403.297162 | 175.3252598 | 3.89804767 |
| 88.25 | 1.540253065 | 195,433.460304 | 1,227.944646 | 175.3525159 | 3.41095735 |
| 88.50 | 1.544616388 | 167,521.444716 | 1,052.568280 | 175.3763662 | 2.92380078 |
| 88.75 | 1.548979711 | 139,606.175338 | 877.171470 | 175.3968104 | 2.43658742 |
| 89.00 | 1.553343034 | 111,688.194356 | 701.757622 | 175.4138479 | 1.94932673 |
| 89.25 | 1.557706357 | 83,768.044017 | 526.330143 | 175.4274784 | 1.46202818 |
| 89.50 | 1.562069681 | 55,846.266619 | 350.892442 | 175.4377015 | 0.97470123 |


| Latitude <br> in <br> Degrees | Latitude in <br> Radians | Radius in Meters <br> of Parallel <br> $\boldsymbol{\rho}(\boldsymbol{\varphi})$ | Circumferen <br> ce in $\mathbf{K m}$ | Difference of <br> Parallels in $\mathbf{K m}$ | Km in a $\boldsymbol{\lambda}$ <br> Degree |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 89.75 | 1.566433004 | $27,923.404494$ | 175.447925 | 175.4445170 | 0.48735535 |
| 90.00 | 1.570796327 | 0.00000 | 0.00000 | 175.4479248 | 0.0000000 |

This could have been done using a numeric integral, which drops the $\varphi$ based terms since $\varphi$ is a constant along a parallel and thereby produces zero to the integral. For example, if $\Delta \varphi=0$, then the $\sqrt{G(\varphi)}$ function is a constant, and the $d \varphi / d t \equiv 0$ which implies

Eq 104. $\quad L_{c}=\int_{a}^{b} \sqrt{E(\varphi)\left(\frac{d \varphi}{d t}\right)^{2}+G(\varphi)\left(\frac{d \lambda}{d t}\right)^{2}} d t$

Eq 105.

$$
E(\varphi)=(M(\varphi))^{2}
$$

$$
\sqrt{E(\varphi)}=M(\varphi)=\frac{a\left(1-e^{2}\right)}{\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2}}
$$

$$
N(\varphi)=\frac{a}{\sqrt{1-e^{2} \sin ^{2} \varphi}} \quad \rho(\varphi)=N(\varphi) \cos \varphi
$$

Eq 106.

$$
\begin{aligned}
G(\varphi) & =N^{2}(\varphi) \cos ^{2} \varphi=\rho^{2}(\varphi)=\left(\frac{a^{2} \cos ^{2} \varphi}{1-e^{2} \sin ^{2} \varphi}\right) \\
\sqrt{G(\varphi)} & =N(\varphi) \cos \varphi=\rho(\varphi)
\end{aligned}
$$

## C. 2 Length of a meridian of north-south latitude

Table 2 below calculates the north-south distances for each quarter degree between $0^{\circ}$ (equator) to $90^{\circ}$ (either pole). Note that the calculations use radians. The function $\mathrm{m}(\varphi)$ describes the radius of curvature along the vertical meridian arcs. The radius of curvature of an arc at a point is the radius of the best-fitting circle tangent to that arc. See Burkholder [4], Wikipedia [33].

$$
\begin{gathered}
M(\varphi)=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2} \\
m\left(\varphi_{n}\right)=\int_{0}^{\varphi_{n}} M(\varphi) d \varphi \cong \sum_{i=1}^{90^{* 4}}\left(\frac{M\left(\varphi_{i}\right)-M\left(\varphi_{i-1}\right)}{2}\right) \Delta \varphi_{i} \\
\Delta \varphi_{i}=\left|\varphi_{i}-\varphi_{i-1}\right|
\end{gathered}
$$

Eq 107.

The same table can be calculated using the length integral in latitudes along a meridian $\int_{0}^{\frac{\pi}{2}} \sqrt{E(\varphi)} d \varphi=$ $\int_{0}^{\frac{\pi}{2}} M(\varphi) d \varphi$; which is described in equation (81. Using a spread sheet to do the calculations, the difference between using $\sqrt{\boldsymbol{E}}$ and $M$ tracked until the end which showed a 0.13 -meter difference, or a little less than 5.1 inches or 13 cm in about $10,001 \mathrm{~km}$. See Latitude, Wikipedia page is https://en.wikipedia.org/wiki/Latitude. Using a different spread sheet with a delta of a tenth of a degree, the difference between $\sqrt{\boldsymbol{E}}$ and $M$ from 0 to 360 degrees was tested; the two were identical to the limits of the application which agreed to 8 decimal places and 7 -digit integer parts meaning that the two values are within 10 nanometers, which would probably mean that the spread sheet was using double precision floating numbers, and found no difference in values. The editor is still working on a proof that then two are mathematical identical functions. The columns are:

1. Degrees: is the current latitude $(\varphi)$ in decimal degrees, in 0.25 increments, beginning at the equator and traversing to either pole.
2. $\mathbf{M}(\boldsymbol{\varphi})$ in meters: This holds the $M(\varphi)$-values for the summation difference between each quarter degree $\left[M\left(\varphi_{i+1}\right)-M\left(\varphi_{i}\right)\right]$ that need to be multiplied by the $\Delta \varphi$ to achieve the delta distance for $M(\varphi)$.
3. KM up to $\varphi_{i}$ : This holds the $i^{\text {th }}$ summation term in meters for the numeric integral e.g. $M\left(\varphi_{n}\right) \cong \sum_{i=1}^{n}\left[M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)\right](\Delta \varphi)$. The first value is null, since each sub-section is the interval between two values of latitude, i.e. the $\Delta \varphi$ 's. This column is the partial sum of the summation, and therefore the current best value for the distance from the equator from 0 to the current $\varphi$ (i.e. $0^{\circ}$ to $0.25^{\circ} . ., 90^{\circ}$ ). The summation in Wikipedia is 10001.965729 km and our value in meters is $10,001,965.7293125$ from the Wikipedia page https://en.wikipedia.org/wiki/Latitude, [32].
4. Delta KM: is the difference since the last partial sum of the numerical integration, and in the light of column 1, the distance between the current $\varphi$ and the directly previous. This is the partial sums that create the previous column.
5. Latitude (Radians): This column lists the angles in radians (needed in the integral) from $0^{\circ}$ to $90^{\circ}$ in quarter degrees or approximately 0.0043633231 radians.
The consistency of these values is based on the size of the interval $0.25^{\circ}$, and the accuracy of the implied linearity in the summation approximation of the integral. Note that the various values are consistent in accuracy for the double precision floating point that is used by the spread sheet. The function $\mathrm{m}(\varphi)$ would be accurate up to 17 significant decimal digits. Table 2 can be trusted for about 9 digits and the result for kilometers for $\varphi$ in $\left[0^{\circ}, 90^{\circ}\right]$, which should be trusted probably to the decimeter, and maybe to the centimeter, so the final distance $10,001.965729313$ is probably correct to 6 decimal places in this example, or more precisely for the ellipsoid. Wikipedia (see
https://en.wikipedia.org/wiki/Latitude, [32]) gives a value (10,001.965729 km) which agrees with the table's value to the millimeter. This is consistent with the delta kilometers between quarter degrees, which is usually near linear at the sub-meter level, which validates the use of only quarter-degree increments and the linear interpolation for the integral $\Delta \varphi_{i}=\left|\varphi_{i}-\varphi_{i-1}\right|=0.25^{\circ}$. The numeric integral using $M(\varphi)$ is in equation Eq 4. More accurate numeric integrals could use a delta of $0.1^{\circ}$; as the limits of double precision numbers is usually set in the $15^{\text {th }}$ or $17^{\text {th }}$ decimal digit. The table below uses 12 decimal digits. See, Weintrit [36] which states $10,001,965.729$ as a best approximation, and references

Bomford, 1985, as one of the best consensus at $10,001,965.72931360$ by looking at Weintrit's assessed 7 best approximations with 4 of them range between 10,001,965.7293127 and 10,001,965.7293136 which puts this calculation within a micrometer of the consensus value. As pointed out earlier, the similar values for " $\lambda$ " is accurate based on the ellipsoid regardless of $\Delta \lambda$. This implies that summations at $\Delta$-angles of a quarter degree $0.25^{\circ}$ ( 0.004363323 radian) or smaller are sufficient to maintain centimeter accuracy or better, using double-precision arithmetic. In the geometries of ISO 19107, most "direct positions" used in coordinate strings will probably much smaller $\Delta$-angles than a quarter degree, which is 27.64 km or larger in latitudes near a pole, approaching 27.9235 km .

Table 2. Length of Meridian Equator to Pole $\int \mathbf{m}(\varphi) \mathbf{d} \varphi$ (or $\sqrt{\mathrm{E}}$ )

| Degree $\varphi$ | $\mathbf{M}(\varphi)$ | KM up to $\varphi$ | delta KM | Radian $=\varphi$ |
| :---: | :---: | :---: | :---: | :---: |
| 0.00 | 6,335,439.32729 | 0 | 0 | 0.000000000 |
| 0.25 | 6,335,440.53848 | 27.643571598 | 27.64357160 | 0.0043633231 |
| 0.50 | 6,335,444.17194 | 55.287153765 | 27.64358217 | 0.0087266463 |
| 0.75 | 6,335,450.22742 | 82.930757070 | 27.64360331 | 0.0130899694 |
| 1.00 | 6,335,458.70445 | 110.574392080 | 27.64363501 | 0.0174532925 |
| 1.25 | 6,335,469.60242 | 138.218069360 | 27.64367728 | 0.0218166156 |
| 1.50 | 6,335,482.92051 | 165.861799471 | 27.64373011 | 0.0261799388 |
| 1.75 | 6,335,498.65773 | 193.505592971 | 27.64379350 | 0.0305432619 |
| 2.00 | 6,335,516.81291 | 221.149460413 | 27.64386744 | 0.0349065850 |
| 2.25 | 6,335,537.38471 | 248.793412344 | 27.64395193 | 0.0392699082 |
| 2.50 | 6,335,560.37161 | 276.437459305 | 27.64404696 | 0.0436332313 |
| 2.75 | 6,335,585.77188 | 304.081611831 | 27.64415253 | 0.0479965544 |
| 3.00 | 6,335,613.58365 | 331.725880447 | 27.64426862 | 0.0523598776 |
| 3.25 | 6,335,643.80485 | 359.370275672 | 27.64439522 | 0.0567232007 |
| 3.50 | 6,335,676.43325 | 387.014808013 | 27.64453234 | 0.0610865238 |
| 3.75 | 6,335,711.46640 | 414.659487969 | 27.64467996 | 0.0654498469 |
| 4.00 | 6,335,748.90172 | 442.304326026 | 27.64483806 | 0.0698131701 |
| 4.25 | 6,335,788.73642 | 469.949332661 | 27.64500663 | 0.0741764932 |
| 4.50 | 6,335,830.96755 | 497.594518335 | 27.64518567 | 0.0785398163 |
| 4.75 | 6,335,875.59196 | 525.239893499 | 27.64537516 | 0.0829031395 |
| 5.00 | 6,335,922.60635 | 552.885468587 | 27.64557509 | 0.0872664626 |
| 5.25 | 6,335,972.00723 | 580.531254021 | 27.64578543 | 0.0916297857 |
| 5.50 | 6,336,023.79091 | 608.177260206 | 27.64600618 | 0.0959931089 |
| 5.75 | 6,336,077.95357 | 635.823497530 | 27.64623732 | 0.1003564320 |
| 6.00 | 6,336,134.49117 | 663.469976364 | 27.64647883 | 0.1047197551 |
| 6.25 | 6,336,193.39951 | 691.116707062 | 27.64673070 | 0.1090830782 |
| 6.50 | 6,336,254.67423 | 718.763699959 | 27.64699290 | 0.1134464014 |
| 6.75 | 6,336,318.31076 | 746.410965370 | 27.64726541 | 0.1178097245 |
| 7.00 | 6,336,384.30438 | 774.058513590 | 27.64754822 | 0.1221730476 |
| 7.25 | 6,336,452.65018 | 801.706354893 | 27.64784130 | 0.1265363708 |
| 7.50 | 6,336,523.34309 | 829.354499531 | 27.64814464 | 0.1308996939 |
| 7.75 | 6,336,596.37786 | 857.002957735 | 27.64845820 | 0.1352630170 |
| 8.00 | 6,336,671.74906 | 884.651739710 | 27.64878198 | 0.1396263402 |


| Degree $\varphi$ | $\mathbf{M}(\varphi)$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 8.25 | 6,336,749.45108 | 912.300855640 | 27.64911593 | 0.1439896633 |
| 8.50 | 6,336,829.47815 | 939.950315681 | 27.64946004 | 0.1483529864 |
| 8.75 | 6,336,911.82433 | 967.600129965 | 27.64981428 | 0.1527163095 |
| 9.00 | 6,336,996.48350 | 995.25308598 | 27.65017863 | 0.1570796327 |
| 9.25 | 6,337,083.44935 | 1,022.900861659 | 27.65055306 | 0.1614429558 |
| 9.50 | 6,337,172.71543 | 1,050.551799199 | 27.65093754 | 0.1658062789 |
| 9.75 | 6,337,264.27510 | 1,078.203131239 | 27.65133204 | 0.1701696021 |
| 10.00 | 6,337,358.12155 | 1,105.854867773 | 27.65173653 | 0.1745329252 |
| 10.25 | 6,337,454.24781 | 1,133.507018763 | 27.65215099 | 0.1788962483 |
| 10.50 | 6,337,552.64673 | 1,161.159594140 | 27.65257538 | 0.1832595715 |
| 10.75 | 6,337,653.31098 | 1,188.812603807 | 27.65300967 | 0.1876228946 |
| 11.00 | 6,337,756.23309 | 1,216.466057630 | 27.65345382 | 0.1919862177 |
| 11.25 | 6,337,861.40539 | 1,244.119965444 | 27.65390781 | 0.1963495408 |
| 11.50 | 6,337,968.82007 | 1,271.774337051 | 27.65437161 | 0.2007128640 |
| 11.75 | 6,338,078.46914 | 1,299.429182218 | 27.65484517 | 0.2050761871 |
| 12.00 | 6,338,190.34443 | 1,327.084510676 | 27.65532846 | 0.2094395102 |
| 12.25 | 6,338,304.43763 | 1,354.740332121 | 27.65582144 | 0.2138028334 |
| 12.50 | 6,338,420.74023 | 1,382.396656212 | 27.65632409 | 0.2181661565 |
| 12.75 | 6,338,539.24360 | 1,410.053492569 | 27.65683636 | 0.2225294796 |
| 13.00 | 6,338,659.93891 | 1,437.710850777 | 27.65735821 | 0.2268928028 |
| 13.25 | 6,338,782.81717 | 1,465.368740381 | 27.65788960 | 0.2312561259 |
| 13.50 | 6,338,907.86925 | 1,493.027170884 | 27.65843050 | 0.2356194490 |
| 13.75 | 6,339,035.08582 | 1,520.686151752 | 27.65898087 | 0.2399827721 |
| 14.00 | 6,339,164.45742 | 1,548.345692409 | 27.65954066 | 0.2443460953 |
| 14.25 | 6,339,295.97442 | 1,576.005802237 | 27.66010983 | 0.2487094184 |
| 14.50 | 6,339,429.62702 | 1,603.666490574 | 27.66068834 | 0.2530727415 |
| 14.75 | 6,339,565.40526 | 1,631.327766719 | 27.66127614 | 0.2574360647 |
| 15.00 | 6,339,703.29904 | 1,658.989639923 | 27.66187320 | 0.2617993878 |
| 15.25 | 6,339,843.29809 | 1,686.652119396 | 27.66247947 | 0.2661627109 |
| 15.50 | 6,339,985.39196 | 1,714.315214300 | 27.66309490 | 0.2705260341 |
| 15.75 | 6,340,129.57009 | 1,741.978933752 | 27.66371945 | 0.2748893572 |
| 16.00 | 6,340,275.82171 | 1,769.643286824 | 27.66435307 | 0.2792526803 |
| 16.25 | 6,340,424.13594 | 1,797.308282539 | 27.66499571 | 0.2836160034 |
| 16.50 | 6,340,574.50172 | 1,824.973929872 | 27.66564733 | 0.2879793266 |
| 16.75 | 6,340,726.90783 | 1,852.640237752 | 27.66630788 | 0.2923426497 |
| 17.00 | 6,340,881.34292 | 1,880.307215055 | 27.66697730 | 0.2967059728 |
| 17.25 | 6,341,037.79548 | 1,907.974870609 | 27.66765555 | 0.3010692960 |
| 17.50 | 6,341,196.25383 | 1,935.643213193 | 27.66834258 | 0.3054326191 |
| 17.75 | 6,341,356.70615 | 1,963.312251532 | 27.66903834 | 0.3097959422 |
| 18.00 | 6,341,519.14049 | 1,990.981994300 | 27.66974277 | 0.3141592654 |
| 18.25 | 6,341,683.54472 | 2,018.652450119 | 27.67045582 | 0.3185225885 |
| 18.50 | 6,341,849.90658 | 2,046.323627558 | 27.67117744 | 0.3228859116 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 18.75 | 6,342,018.21365 | 2,073.995535131 | 27.67190757 | 0.3272492347 |
| 19.00 | 6,342,188.45337 | 2,101.668181299 | 27.67264617 | 0.3316125579 |
| 19.25 | 6,342,360.61304 | 2,129.341574467 | 27.67339317 | 0.3359758810 |
| 19.50 | 6,342,534.67980 | 2,157.015722983 | 27.67414852 | 0.3403392041 |
| 19.75 | 6,342,710.64066 | 2,184.690635141 | 27.67491216 | 0.3447025273 |
| 20.00 | 6,342,888.48248 | 2,212.366319177 | 27.67568404 | 0.3490658504 |
| 20.25 | 6,343,068.19198 | 2,240.042783269 | 27.67646409 | 0.3534291735 |
| 20.50 | 6,343,249.75573 | 2,267.720035537 | 27.67725227 | 0.3577924967 |
| 20.75 | 6,343,433.16018 | 2,295.398084042 | 27.67804850 | 0.3621558198 |
| 21.00 | 6,343,618.39162 | 2,323.076936785 | 27.67885274 | 0.3665191429 |
| 21.25 | 6,343,805.43621 | 2,350.756601709 | 27.67966492 | 0.3708824660 |
| 21.50 | 6,343,994.27996 | 2,378.437086694 | 27.68048499 | 0.3752457892 |
| 21.75 | 6,344,184.90878 | 2,406.118399560 | 27.68131287 | 0.3796091123 |
| 22.00 | 6,344,377.30840 | 2,433.800548064 | 27.68214850 | 0.3839724354 |
| 22.25 | 6,344,571.46444 | 2,461.483539902 | 27.68299184 | 0.3883357586 |
| 22.50 | 6,344,767.36237 | 2,489.167382706 | 27.68384280 | 0.3926990817 |
| 22.75 | 6,344,964.98756 | 2,516.852084044 | 27.68470134 | 0.3970624048 |
| 23.00 | 6,345,164.32522 | 2,544.537651420 | 27.68556738 | 0.4014257280 |
| 23.25 | 6,345,365.36042 | 2,572.224092275 | 27.68644085 | 0.4057890511 |
| 23.50 | 6,345,568.07814 | 2,599.911413982 | 27.68732171 | 0.4101523742 |
| 23.75 | 6,345,772.46320 | 2,627.599623849 | 27.68820987 | 0.4145156973 |
| 24.00 | 6,345,978.5029 | 2,655.288729118 | 27.68910527 | 0.4188790205 |
| 24.25 | 6,346,186.17400 | 2,682.978736965 | 27.69000785 | 0.4232423436 |
| 24.50 | 6,346,395.46878 | 2,710.669654495 | 27.69091753 | 0.4276056667 |
| 24.75 | 6,346,606.36895 | 2,738.361488749 | 27.69183425 | 0.4319689899 |
| 25.00 | 6,346,818.85872 | 2,766.054246697 | 27.69275795 | 0.4363323130 |
| 25.25 | 6,347,032.92217 | 2,793.747935239 | 27.69368854 | 0.4406956361 |
| 25.50 | 6,347,248.54325 | 2,821.442561207 | 27.69462597 | 0.4450589593 |
| 25.75 | 6,347,465.70581 | 2,849.138131363 | 27.69557016 | 0.4494222824 |
| 26.00 | 6,347,684.39358 | 2,876.834652396 | 27.69652103 | 0.4537856055 |
| 26.25 | 6,347,904.59016 | 2,904.532130927 | 27.69747853 | 0.4581489286 |
| 26.50 | 6,348,126.27904 | 2,932.230573502 | 27.69844258 | 0.4625122518 |
| 26.75 | 6,348,349.44360 | 2,959.929986597 | 27.69941309 | 0.4668755749 |
| 27.00 | 6,348,574.06710 | 2,987.630376614 | 27.70039002 | 0.4712388980 |
| 27.25 | 6,348,800.13268 | 3,015.331749882 | 27.70137327 | 0.4756022212 |
| 27.50 | 6,349,027.62339 | 3,043.034112657 | 27.70236277 | 0.4799655443 |
| 27.75 | 6,349,256.52215 | 3,070.737471118 | 27.70335846 | 0.4843288674 |
| 28.00 | 6,349,486.81178 | 3,098.441831374 | 27.70436026 | 0.4886921906 |
| 28.25 | 6,349,718.47500 | 3,126.147199454 | 27.70536808 | 0.4930555137 |
| 28.50 | 6,349,951.49441 | 3,153.853581314 | 27.70638186 | 0.4974188368 |
| 28.75 | 6,350,185.85252 | 3,181.560982834 | 27.70740152 | 0.5017821599 |
| 29.00 | 6,350,421.53171 | 3,209.269409816 | 27.70842698 | 0.5061454831 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\varphi$ |
| :---: | :---: | :---: | :---: | :---: |
| 29.25 | 6,350,658.51428 | 3,236.978867986 | 27.70945817 | 0.5105088062 |
| 29.50 | 6,350,896.78242 | 3,264.689362993 | 27.71049501 | 0.5148721293 |
| 29.75 | 6,351,136.31824 | 3,292.400900406 | 27.71153741 | 0.5192354525 |
| 30.00 | 6,351,377.10372 | 3,320.113485717 | 27.71258531 | 0.5235987756 |
| 30.25 | 6,351,619.12075 | 3,347.827124341 | 27.71363862 | 0.5279620987 |
| 30.50 | 6,351,862.35115 | 3,375.541821609 | 27.71469727 | 0.5323254219 |
| 30.75 | 6,352,106.77661 | 3,403.257582778 | 27.71576117 | 0.5366887450 |
| 31.00 | 6,352,352.37875 | 3,430.974413022 | 27.71683024 | 0.5410520681 |
| 31.25 | 6,352,599.13909 | 3,458.692317433 | 27.71790441 | 0.5454153912 |
| 31.50 | 6,352,847.03906 | 3,486.411301026 | 27.71898359 | 0.5497787144 |
| 31.75 | 6,353,096.05999 | 3,514.131368732 | 27.72006771 | 0.5541420375 |
| 32.00 | 6,353,346.18315 | 3,541.852525402 | 27.72115667 | 0.5585053606 |
| 32.25 | 6,353,597.38969 | 3,569.574775803 | 27.72225040 | 0.5628686838 |
| 32.50 | 6,353,849.66071 | 3,597.298124622 | 27.72334882 | 0.5672320069 |
| 32.75 | 6,354,102.97718 | 3,625.022576462 | 27.72445184 | 0.5715953300 |
| 33.00 | 6,354,357.32003 | 3,652.748135843 | 27.72555938 | 0.5759586532 |
| 33.25 | 6,354,612.67009 | 3,680.474807201 | 27.72667136 | 0.5803219763 |
| 33.50 | 6,354,869.00812 | 3,708.202594889 | 27.72778769 | 0.5846852994 |
| 33.75 | 6,355,126.31478 | 3,735.931503177 | 27.72890829 | 0.5890486225 |
| 34.00 | 6,355,384.57067 | 3,763.661536247 | 27.73003307 | 0.5934119457 |
| 34.25 | 6,355,643.75632 | 3,791.392698199 | 27.73116195 | 0.5977752688 |
| 34.50 | 6,355,903.85217 | 3,819.124993048 | 27.73229485 | 0.6021385919 |
| 34.75 | 6,356,164.83860 | 3,846.858424723 | 27.73343167 | 0.6065019151 |
| 35.00 | 6,356,426.69592 | 3,874.592997065 | 27.73457234 | 0.6108652382 |
| 35.25 | 6,356,689.40435 | 3,902.328713832 | 27.73571677 | 0.6152285613 |
| 35.50 | 6,356,952.94406 | 3,930.065578695 | 27.73686486 | 0.6195918845 |
| 35.75 | 6,357,217.29515 | 3,957.803595236 | 27.73801654 | 0.6239552076 |
| 36.00 | 6,357,482.43765 | 3,985.542766954 | 27.73917172 | 0.6283185307 |
| 36.25 | 6,357,748.35154 | 4,013.283097257 | 27.74033030 | 0.6326818538 |
| 36.50 | 6,358,015.01671 | 4,041.024589467 | 27.74149221 | 0.6370451770 |
| 36.75 | 6,358,282.41302 | 4,068.767246818 | 27.74265735 | 0.6414085001 |
| 37.00 | 6,358,550.52026 | 4,096.511072457 | 27.74382564 | 0.6457718232 |
| 37.25 | 6,358,819.31814 | 4,124.256069441 | 27.74499698 | 0.6501351464 |
| 37.50 | 6,359,088.78634 | 4,152.002240740 | 27.74617130 | 0.6544984695 |
| 37.75 | 6,359,358.90448 | 4,179.749589233 | 27.74734849 | 0.6588617926 |
| 38.00 | 6,359,629.65213 | 4,207.498117713 | 27.74852848 | 0.6632251158 |
| 38.25 | 6,359,901.00878 | 4,235.247828881 | 27.74971117 | 0.6675884389 |
| 38.50 | 6,360,172.95391 | 4,262.998725349 | 27.75089647 | 0.6719517620 |
| 38.75 | 6,360,445.46692 | 4,290.750809641 | 27.75208429 | 0.6763150851 |
| 39.00 | 6,360,718.52718 | 4,318.504084188 | 27.75327455 | 0.6806784083 |
| 39.25 | 6,360,992.11401 | 4,346.258551335 | 27.75446715 | 0.6850417314 |
| 39.50 | 6,361,266.20668 | 4,374.014213333 | 27.75566200 | 0.6894050545 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\varphi$ |
| :---: | :---: | :---: | :---: | :---: |
| 39.75 | 6,361,540.78443 | 4,401.771072345 | 27.75685901 | 0.6937683777 |
| 40.00 | 6,361,815.82643 | 4,429.529130440 | 27.75805810 | 0.6981317008 |
| 40.25 | 6,362,091.31185 | 4,457.288389601 | 27.75925916 | 0.7024950239 |
| 40.50 | 6,362,367.21980 | 4,485.048851714 | 27.76046211 | 0.7068583471 |
| 40.75 | 6,362,643.52934 | 4,512.810518580 | 27.76166687 | 0.7112216702 |
| 41.00 | 6,362,920.21953 | 4,540.573391904 | 27.76287332 | 0.7155849933 |
| 41.25 | 6,363,197.26936 | 4,568.337473301 | 27.76408140 | 0.7199483164 |
| 41.50 | 6,363,474.65782 | 4,596.102764295 | 27.76529099 | 0.7243116396 |
| 41.75 | 6,363,752.36385 | 4,623.869266317 | 27.76650202 | 0.7286749627 |
| 42.00 | 6,364,030.36636 | 4,651.636980707 | 27.76771439 | 0.7330382858 |
| 42.25 | 6,364,308.64425 | 4,679.405908713 | 27.76892801 | 0.7374016090 |
| 42.50 | 6,364,587.17637 | 4,707.176051489 | 27.77014278 | 0.7417649321 |
| 42.75 | 6,364,865.94158 | 4,734.947410100 | 27.77135861 | 0.7461282552 |
| 43.00 | 6,365,144.91867 | 4,762.719985516 | 27.77257542 | 0.7504915784 |
| 43.25 | 6,365,424.08646 | 4,790.493778615 | 27.77379310 | 0.7548549015 |
| 43.50 | 6,365,703.42372 | 4,818.268790183 | 27.77501157 | 0.7592182246 |
| 43.75 | 6,365,982.90920 | 4,846.045020913 | 27.77623073 | 0.7635815477 |
| 44.00 | 6,366,262.52166 | 4,873.822471405 | 27.77745049 | 0.7679448709 |
| 44.25 | 6,366,542.23982 | 4,901.601142168 | 27.77867076 | 0.7723081940 |
| 44.50 | 6,366,822.04239 | 4,929.381033616 | 27.77989145 | 0.7766715171 |
| 44.75 | 6,367,101.90810 | 4,957.162146070 | 27.78111245 | 0.7810348403 |
| 45.00 | 6,367,381.81562 | 4,984.944479760 | 27.78233369 | 0.7853981634 |
| 45.25 | 6,367,661.74365 | 5,012.728034822 | 27.78355506 | 0.7897614865 |
| 45.50 | 6,367,941.67088 | 5,040.512811298 | 27.78477648 | 0.7941248097 |
| 45.75 | 6,368,221.57597 | 5,068.298809139 | 27.78599784 | 0.7984881328 |
| 46.00 | 6,368,501.43760 | 5,096.086028202 | 27.78721906 | 0.8028514559 |
| 46.25 | 6,368,781.23446 | 5,123.874468250 | 27.78844005 | 0.8072147790 |
| 46.50 | 6,369,060.94520 | 5,151.664128954 | 27.78966070 | 0.8115781022 |
| 46.75 | 6,369,340.54851 | 5,179.455009893 | 27.79088094 | 0.8159414253 |
| 47.00 | 6,369,620.02306 | 5,207.247110550 | 27.79210066 | 0.8203047484 |
| 47.25 | 6,369,899.34754 | 5,235.040430317 | 27.79331977 | 0.8246680716 |
| 47.50 | 6,370,178.5064 | 5,262.834968493 | 27.79453818 | 0.8290313947 |
| 47.75 | 6,370,457.46105 | 5,290.630724284 | 27.79575579 | 0.8333947178 |
| 48.00 | 6,370,736.20750 | 5,318.427696803 | 27.79697252 | 0.8377580410 |
| 48.25 | 6,371,014.71869 | 5,346.225885070 | 27.79818827 | 0.8421213641 |
| 48.50 | 6,371,292.97336 | 5,374.025288011 | 27.79940294 | 0.8464846872 |
| 48.75 | 6,371,570.95027 | 5,401.825904461 | 27.80061645 | 0.8508480103 |
| 49.00 | 6,371,848.62817 | 5,429.627733162 | 27.80182870 | 0.8552113335 |
| 49.25 | 6,372,125.98585 | 5,457.430772762 | 27.80303960 | 0.8595746566 |
| 49.50 | 6,372,403.00212 | 5,485.235021819 | 27.80424906 | 0.8639379797 |
| 49.75 | 6,372,679.65580 | 5,513.040478797 | 27.80545698 | 0.8683013029 |
| 50.00 | 6,372,955.92574 | 5,540.847142066 | 27.80666327 | 0.8726646260 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 50.25 | 6,373,231.79080 | 5,568.655009908 | 27.80786784 | 0.8770279491 |
| 50.50 | 6,373,507.22990 | 5,596.464080508 | 27.80907060 | 0.8813912723 |
| 50.75 | 6,373,782.22196 | 5,624.274351963 | 27.81027145 | 0.8857545954 |
| 51.00 | 6,374,056.74594 | 5,652.085822276 | 27.81147031 | 0.8901179185 |
| 51.25 | 6,374,330.78082 | 5,679.898489359 | 27.81266708 | 0.8944812416 |
| 51.50 | 6,374,604.30562 | 5,707.712351032 | 27.81386167 | 0.8988445648 |
| 51.75 | 6,374,877.29941 | 5,735.527405023 | 27.81505399 | 0.9032078879 |
| 52.00 | 6,375,149.74128 | 5,763.343648970 | 27.81624395 | 0.9075712110 |
| 52.25 | 6,375,421.61034 | 5,791.161080420 | 27.81743145 | 0.9119345342 |
| 52.50 | 6,375,692.88579 | 5,818.979696827 | 27.81861641 | 0.9162978573 |
| 52.75 | 6,375,963.54682 | 5,846.799495556 | 27.81979873 | 0.9206611804 |
| 53.00 | 6,376,233.57268 | 5,874.620473881 | 27.82097832 | 0.9250245036 |
| 53.25 | 6,376,502.94269 | 5,902.442628985 | 27.82215510 | 0.9293878267 |
| 53.50 | 6,376,771.63617 | 5,930.265957961 | 27.82332898 | 0.9337511498 |
| 53.75 | 6,377,039.63252 | 5,958.090457813 | 27.82449985 | 0.9381144729 |
| 54.00 | 6,377,306.91119 | 5,985.916125454 | 27.82566764 | 0.9424777961 |
| 54.25 | 6,377,573.45166 | 6,013.742957708 | 27.82683225 | 0.9468411192 |
| 54.50 | 6,377,839.23347 | 6,041.570951309 | 27.82799360 | 0.9512044423 |
| 54.75 | 6,378,104.23622 | 6,069.400102902 | 27.82915159 | 0.9555677655 |
| 55.00 | 6,378,368.43958 | 6,097.230409043 | 27.83030614 | 0.9599310886 |
| 55.25 | 6,378,631.82324 | 6,125.061866201 | 27.83145716 | 0.9642944117 |
| 55.50 | 6,378,894.36697 | 6,152.894470755 | 27.83260455 | 0.9686577349 |
| 55.75 | 6,379,156.05061 | 6,180.728218995 | 27.83374824 | 0.9730210580 |
| 56.00 | 6,379,416.85404 | 6,208.563107125 | 27.83488813 | 0.9773843811 |
| 56.25 | 6,379,676.75723 | 6,236.399131261 | 27.83602414 | 0.9817477042 |
| 56.50 | 6,379,935.74019 | 6,264.236287431 | 27.83715617 | 0.9861110274 |
| 56.75 | 6,380,193.78300 | 6,292.074571576 | 27.83828415 | 0.9904743505 |
| 57.00 | 6,380,450.86583 | 6,319.913979551 | 27.83940797 | 0.9948376736 |
| 57.25 | 6,380,706.96889 | 6,347.754507124 | 27.84052757 | 0.9992009968 |
| 57.50 | 6,380,962.07249 | 6,375.596149977 | 27.84164285 | 1.0035643199 |
| 57.75 | 6,381,216.15699 | 6,403.438903705 | 27.84275373 | 1.0079276430 |
| 58.00 | 6,381,469.20284 | 6,431.282763821 | 27.84386012 | 1.0122909662 |
| 58.25 | 6,381,721.19056 | 6,459.127725749 | 27.84496193 | 1.0166542893 |
| 58.50 | 6,381,972.10074 | 6,486.973784830 | 27.84605908 | 1.0210176124 |
| 58.75 | 6,382,221.91407 | 6,514.820936320 | 27.84715149 | 1.0253809355 |
| 59.00 | 6,382,470.61129 | 6,542.669175392 | 27.84823907 | 1.0297442587 |
| 59.25 | 6,382,718.17325 | 6,570.518497133 | 27.84932174 | 1.0341075818 |
| 59.50 | 6,382,964.58087 | 6,598.368896548 | 27.85039942 | 1.0384709049 |
| 59.75 | 6,383,209.81517 | 6,626.220368560 | 27.85147201 | 1.0428342281 |
| 60.00 | 6,383,453.85723 | 6,654.072908008 | 27.85253945 | 1.0471975512 |
| 60.25 | 6,383,696.68824 | 6,681.926509647 | 27.85360164 | 1.0515608743 |
| 60.50 | 6,383,938.28948 | 6,709.781168154 | 27.85465851 | 1.0559241975 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 60.75 | 6,384,178.64230 | 6,737.636878121 | 27.85570997 | 1.0602875206 |
| 61.00 | 6,384,417.72818 | 6,765.493634062 | 27.85675594 | 1.0646508437 |
| 61.25 | 6,384,655.52865 | 6,793.351430407 | 27.85779635 | 1.0690141668 |
| 61.50 | 6,384,892.02537 | 6,821.210261508 | 27.85883110 | 1.0733774900 |
| 61.75 | 6,385,127.20009 | 6,849.070121636 | 27.85986013 | 1.0777408131 |
| 62.00 | 6,385,361.03464 | 6,876.931004984 | 27.86088335 | 1.0821041362 |
| 62.25 | 6,385,593.51098 | 6,904.792905664 | 27.86190068 | 1.0864674594 |
| 62.50 | 6,385,824.61114 | 6,932.655817712 | 27.86291205 | 1.0908307825 |
| 62.75 | 6,386,054.31727 | 6,960.519735083 | 27.86391737 | 1.0951941056 |
| 63.00 | 6,386,282.61164 | 6,988.384651656 | 27.86491657 | 1.0995574288 |
| 63.25 | 6,386,509.47659 | 7,016.25561232 | 27.86590958 | 1.1039207519 |
| 63.50 | 6,386,734.89460 | 7,044.117457537 | 27.86689630 | 1.1082840750 |
| 63.75 | 6,386,958.84824 | 7,071.985334219 | 27.86787668 | 1.1126473981 |
| 64.00 | 6,387,181.32020 | 7,099.854184850 | 27.86885063 | 1.1170107213 |
| 64.25 | 6,387,402.29327 | 7,127.724002929 | 27.86981808 | 1.1213740444 |
| 64.50 | 6,387,621.75037 | 7,155.594781876 | 27.87077895 | 1.1257373675 |
| 64.75 | 6,387,839.67451 | 7,183.466515042 | 27.87173317 | 1.1301006907 |
| 65.00 | 6,388,056.04884 | 7,211.339195700 | 27.87268066 | 1.1344640138 |
| 65.25 | 6,388,270.85661 | 7,239.212817051 | 27.87362135 | 1.1388273369 |
| 65.50 | 6,388,484.08121 | 7,267.087372225 | 27.87455517 | 1.1431906601 |
| 65.75 | 6,388,695.70612 | 7,294.962854276 | 27.87548205 | 1.1475539832 |
| 66.00 | 6,388,905.71497 | 7,322.839256189 | 27.87640191 | 1.1519173063 |
| 66.25 | 6,389,114.09149 | 7,350.716570877 | 27.87731469 | 1.1562806294 |
| 66.50 | 6,389,320.81954 | 7,378.594791183 | 27.87822031 | 1.1606439526 |
| 66.75 | 6,389,525.88312 | 7,406.473909880 | 27.87911870 | 1.1650072757 |
| 67.00 | 6,389,729.26633 | 7,434.353919668 | 27.88000979 | 1.1693705988 |
| 67.25 | 6,389,930.95343 | 7,462.234813184 | 27.88089352 | 1.1737339220 |
| 67.50 | 6,390,130.92877 | 7,490.116582990 | 27.88176981 | 1.1780972451 |
| 67.75 | 6,390,329.17687 | 7,517.999221586 | 27.88263860 | 1.1824605682 |
| 68.00 | 6,390,525.68235 | 7,545.882721400 | 27.88349981 | 1.1868238914 |
| 68.25 | 6,390,720.42998 | 7,573.767074796 | 27.88435340 | 1.1911872145 |
| 68.50 | 6,390,913.40466 | 7,601.652274071 | 27.88519927 | 1.1955505376 |
| 68.75 | 6,391,104.59142 | 7,629.538311456 | 27.88603739 | 1.1999138607 |
| 69.00 | 6,391,293.97544 | 7,657.425179117 | 27.88686766 | 1.2042771839 |
| 69.25 | 6,391,481.54202 | 7,685.312869158 | 27.88769004 | 1.2086405070 |
| 69.50 | 6,391,667.27661 | 7,713.201373615 | 27.88850446 | 1.2130038301 |
| 69.75 | 6,391,851.16480 | 7,741.090684464 | 27.88931085 | 1.2173671533 |
| 70.00 | 6,392,033.19232 | 7,768.980793617 | 27.89010915 | 1.2217304764 |
| 70.25 | 6,392,213.34504 | 7,796.871692925 | 27.89089931 | 1.2260937995 |
| 70.50 | 6,392,391.60897 | 7,824.763374177 | 27.89168125 | 1.2304571227 |
| 70.75 | 6,392,567.97028 | 7,852.655829101 | 27.89245492 | 1.2348204458 |
| 71.00 | 6,392,742.41526 | 7,880.549049366 | 27.89322026 | 1.2391837689 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 71.25 | 6,392,914.93037 | 7,908.443026580 | 27.89397721 | 1.2435470920 |
| 71.50 | 6,393,085.50222 | 7,936.337752293 | 27.89472571 | 1.2479104152 |
| 71.75 | 6,393,254.11755 | 7,964.233217999 | 27.89546571 | 1.2522737383 |
| 72.00 | 6,393,420.76326 | 7,992.129415130 | 27.89619713 | 1.2566370614 |
| 72.25 | 6,393,585.42640 | 8,020.026335066 | 27.89691994 | 1.2610003846 |
| 72.50 | 6,393,748.09418 | 8,047.923969126 | 27.89763406 | 1.2653637077 |
| 72.75 | 6,393,908.75395 | 8,075.822308578 | 27.89833945 | 1.2697270308 |
| 73.00 | 6,394,067.39323 | 8,103.721344633 | 27.89903605 | 1.2740903540 |
| 73.25 | 6,394,223.99968 | 8,131.621068446 | 27.89972381 | 1.2784536771 |
| 73.50 | 6,394,378.56112 | 8,159.521471123 | 27.90040268 | 1.2828170002 |
| 73.75 | 6,394,531.06554 | 8,187.422543714 | 27.90107259 | 1.2871803233 |
| 74.00 | 6,394,681.50108 | 8,215.324277217 | 27.90173350 | 1.2915436465 |
| 74.25 | 6,394,829.85604 | 8,243.226662580 | 27.90238536 | 1.2959069696 |
| 74.50 | 6,394,976.11887 | 8,271.129690699 | 27.90302812 | 1.3002702927 |
| 74.75 | 6,395,120.27820 | 8,299.033352421 | 27.90366172 | 1.3046336159 |
| 75.00 | 6,395,262.32281 | 8,326.937638543 | 27.90428612 | 1.3089969390 |
| 75.25 | 6,395,402.24164 | 8,354.842539814 | 27.90490127 | 1.3133602621 |
| 75.50 | 6,395,540.02382 | 8,382.748046935 | 27.90550712 | 1.3177235853 |
| 75.75 | 6,395,675.65861 | 8,410.654150559 | 27.90610362 | 1.3220869084 |
| 76.00 | 6,395,809.13546 | 8,438.560841293 | 27.90669073 | 1.3264502315 |
| 76.25 | 6,395,940.44398 | 8,466.468109700 | 27.90726841 | 1.3308135546 |
| 76.50 | 6,396,069.57394 | 8,494.375946295 | 27.90783660 | 1.3351768778 |
| 76.75 | 6,396,196.51529 | 8,522.284341551 | 27.90839526 | 1.3395402009 |
| 77.00 | 6,396,321.25815 | 8,550.193285897 | 27.90894435 | 1.3439035240 |
| 77.25 | 6,396,443.79280 | 8,578.102769718 | 27.90948382 | 1.3482668472 |
| 77.50 | 6,396,564.10969 | 8,606.012783360 | 27.91001364 | 1.3526301703 |
| 77.75 | 6,396,682.19946 | 8,633.923317124 | 27.91053376 | 1.3569934934 |
| 78.00 | 6,396,798.05290 | 8,661.834361273 | 27.91104415 | 1.3613568166 |
| 78.25 | 6,396,911.66099 | 8,689.745906029 | 27.91154476 | 1.3657201397 |
| 78.50 | 6,397,023.01488 | 8,717.657941577 | 27.91203555 | 1.3700834628 |
| 78.75 | 6,397,132.10589 | 8,745.570458060 | 27.91251648 | 1.3744467859 |
| 79.00 | 6,397,238.92553 | 8,773.483445588 | 27.91298753 | 1.3788101091 |
| 79.25 | 6,397,343.46545 | 8,801.396894230 | 27.91344864 | 1.3831734322 |
| 79.50 | 6,397,445.71753 | 8,829.310794023 | 27.91389979 | 1.3875367553 |
| 79.75 | 6,397,545.67378 | 8,857.225134966 | 27.91434094 | 1.3919000785 |
| 80.00 | 6,397,643.32642 | 8,885.139907025 | 27.91477206 | 1.3962634016 |
| 80.25 | 6,397,738.66783 | 8,913.055100131 | 27.91519311 | 1.4006267247 |
| 80.50 | 6,397,831.69058 | 8,940.970704184 | 27.91560405 | 1.4049900479 |
| 80.75 | 6,397,922.38741 | 8,968.886709051 | 27.91600487 | 1.4093533710 |
| 81.00 | 6,398,010.75127 | 8,996.803104568 | 27.91639552 | 1.4137166941 |
| 81.25 | 6,398,096.77524 | 9,024.719880540 | 27.91677597 | 1.4180800172 |
| 81.50 | 6,398,180.45263 | 9,052.637026743 | 27.91714620 | 1.4224433404 |


| Degree $\varphi$ | $\mathbf{M ( \varphi )}$ | KM up to $\varphi$ | delta KM | Radian= $\boldsymbol{\varphi}$ |
| :---: | :---: | :---: | :---: | :---: |
| 81.75 | 6,398,261.77691 | 9,080.554532924 | 27.91750618 | 1.4268066635 |
| 82.00 | 6,398,340.74173 | 9,108.472388801 | 27.91785588 | 1.4311699866 |
| 82.25 | 6,398,417.34095 | 9,136.390584067 | 27.91819527 | 1.4355333098 |
| 82.50 | 6,398,491.56857 | 9,164.309108385 | 27.91852432 | 1.4398966329 |
| 82.75 | 6,398,563.41881 | 9,192.227951396 | 27.91884301 | 1.4442599560 |
| 83.00 | 6,398,632.88607 | 9,220.147102714 | 27.91915132 | 1.4486232792 |
| 83.25 | 6,398,699.96493 | 9,248.066551930 | 27.91944922 | 1.4529866023 |
| 83.50 | 6,398,764.65015 | 9,275.986288610 | 27.91973668 | 1.4573499254 |
| 83.75 | 6,398,826.93668 | 9,303.906302299 | 27.92001369 | 1.4617132485 |
| 84.00 | 6,398,886.81967 | 9,331.826582521 | 27.92028022 | 1.4660765717 |
| 84.25 | 6,398,944.29444 | 9,359.747118778 | 27.92053626 | 1.4704398948 |
| 84.50 | 6,398,999.35651 | 9,387.667900553 | 27.92078177 | 1.4748032179 |
| 84.75 | 6,399,052.00158 | 9,415.588917307 | 27.92101675 | 1.4791665411 |
| 85.00 | 6,399,102.22554 | 9,443.510158487 | 27.92124118 | 1.4835298642 |
| 85.25 | 6,399,150.02446 | 9,471.431613520 | 27.92145503 | 1.4878931873 |
| 85.50 | 6,399,195.39464 | 9,499.353271817 | 27.92165830 | 1.4922565105 |
| 85.75 | 6,399,238.33250 | 9,527.275122771 | 27.92185095 | 1.4966198336 |
| 86.00 | 6,399,278.83472 | 9,555.197155764 | 27.92203299 | 1.509831567 |
| 86.25 | 6,399,316.89812 | 9,583.119360160 | 27.92220440 | 1.5053464798 |
| 86.50 | 6,399,352.51974 | 9,611.041725312 | 27.92236515 | 1.5097098030 |
| 86.75 | 6,399,385.69680 | 9,638.964240560 | 27.92251525 | 1.5140731261 |
| 87.00 | 6,399,416.42669 | 9,666.886895230 | 27.92265467 | 1.5184364492 |
| 87.25 | 6,399,444.70703 | 9,694.809678641 | 27.92278341 | 1.5227997724 |
| 87.50 | 6,399,470.53561 | 9,722.732580100 | 27.92290146 | 1.5271630955 |
| 87.75 | 6,399,493.91041 | 9,750.655588904 | 27.92300880 | 1.5315264186 |
| 88.00 | 6,399,514.82961 | 9,778.578694342 | 27.92310544 | 1.5358897418 |
| 88.25 | 6,399,533.29157 | 9,806.501885696 | 27.92319135 | 1.5402530649 |
| 88.50 | 6,399,549.29485 | 9,834.425152242 | 27.92326655 | 1.5446163880 |
| 88.75 | 6,399,562.83820 | 9,862.348483249 | 27.92333101 | 1.5489797111 |
| 89.00 | 6,399,573.92057 | 9,890.271867981 | 27.92338473 | 1.5533430343 |
| 89.25 | 6,399,582.54108 | 9,918.195295697 | 27.92342772 | 1.5577063574 |
| 89.50 | 6,399,588.69908 | 9,946.118755656 | 27.92345996 | 1.5620696805 |
| 89.75 | 6,399,592.39406 | 9,974.042237110 | 27.92348145 | 1.5664330037 |
| 90.00 | 6,399,593.62576 | 10,001.965729313 | 27.92349220 | 1.5707963268 |

The most accurate value taken in Weintrit, [36], is $10,001,965.72931270 \mathrm{~m}$ which is consistent with the above $10,001,965.72931260 \mathrm{~m}$ to the micrometer $\left(10^{-6}\right)$. This implies that our Trapezoid-rule calculations in meters on a meridian is valid and sufficiently accurate for GIS use. This is also consistent with the Wikipedia "Latitude" entry which cites $10,001.965729 \mathrm{~km}$ (see [32]). The Simpson rule method is described in [37]. Simpson rule summation is a bit more accurate, but the Trapezoid rule works sufficiently for the needs of GIS accuracy using quarter degree latitude steps.

The accuracy for east-west parallel for longitude does not need the numeric integration, and so it simply trigonometric functions is probably more accurate than along meridians.

## C. 3 Area of a Surface

The area integral is like the length integrals, except instead of using Pythagorean summation, it multiplies horizontal $\lambda$-distances and vertical to get area in square meters. Essentially, the area locally for a $\Delta \Phi, \Delta \Lambda$ rectangle (the minimum bounding rectangle) which is divided into horizontal stripes and then intersected with the area geometry. This gives a set of sub-strips where the boundary of the area crosses the stripe. This gives us a set of horizontal sections of lengths " $\Delta \lambda_{1, j}, \Delta \lambda_{2, j}, \ldots, \Delta \lambda_{n_{i}-1, j}, \Delta \lambda_{n_{i}, j}$ " for the latitude division lines $\varphi_{0}, \varphi_{1}, \ldots, \varphi_{m} ; 0, \ldots, j, \ldots m$ with $\Delta \varphi_{j}=\varphi_{j}-\varphi_{j-1}$ and a single vertical height for each stripe $\Delta \varphi_{j}$.

For each sub-stripe, the area integral is the product of the corresponding meter distance which is exactly what you do with length, but this time you multiply to get local areas and then add the little strips into a total area. An example is in Table 3.

Eq 108.

$$
\begin{gathered}
A_{S}=\iint_{W} \sqrt{E G} d \varphi d \lambda \\
E(\varphi)=\left(\mathrm{N}^{\prime}(\varphi) \cos \varphi+\mathrm{N}(\varphi) \sin \varphi\right)^{2}+\frac{b^{4}}{a^{4}}\left(\mathrm{~N}^{\prime}(\varphi) \sin \varphi+\mathrm{N}(\varphi) \cos \varphi\right)^{2} \\
=M^{2}(\varphi)=\left[a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2}\right]^{2} \\
\mathrm{G}(\varphi)=\mathrm{N}(\varphi)^{2} \cos ^{2} \varphi=\rho^{2}(\varphi)
\end{gathered}
$$

$$
\begin{gathered}
\mathrm{G}(\varphi)=\mathrm{N}(\varphi)^{2} \cos ^{2} \varphi=\rho^{2}(\varphi) \\
\sqrt{E(\varphi)}=M(\varphi)=a\left(1-e^{2}\right)\left(1-e^{2} \sin ^{2} \varphi\right)^{-3 / 2} \\
\sqrt{G(\varphi)}=\rho(\varphi)=\mathrm{N}(\varphi) \cos \varphi \\
A_{S}=\sum\left[\left(M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)\right) \Delta \varphi_{i}\right]\left[\left(\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)\right) \Delta \lambda_{i}\right]
\end{gathered}
$$

For each stripe " $j$ " of height $\Delta \varphi_{j}$ there are sub-stips of lengths $\Delta \lambda_{1, j}, \Delta \lambda_{2, j}, \ldots, \Delta \lambda_{n_{i}-1, j}, \Delta \lambda_{n_{i}, j}$

Eq 109.

$$
\Delta \lambda_{j}=\sum_{i=1}^{n_{i}} \Delta \lambda_{i, j} \text { with area }=[\text { height }] \times[\text { length }]:
$$

$$
A \cong\left[\sum_{j=1}^{m}\left(\frac{M\left(\varphi_{j}\right)+M\left(\varphi_{j-1}\right)}{2}\right) \Delta \varphi_{j}\right]\left[\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2}\right)\left(\Delta \lambda_{j}\right)\right]
$$

In the numeric approximation for the area integral is a double summation, both in the latitude and the longitude directions. The table below expresses angles as degrees, but the units of latitude and longitude are in radians in the integrals.

$$
\begin{aligned}
& \varphi_{i=0 . .8}=\{0,0.125,0.250,0.375,0.5,0.625,0.750,0.875,1.00\} ; \Delta \varphi_{i}=\varphi_{i}-\varphi_{i-1} \\
& \lambda_{j=0.8}=\{0,0.125,0.250,0.375,0.5,0.625,0.750,0.875 .1 .00\} ; \Delta \lambda_{i}=\lambda_{i}-\lambda_{i-1}=0.125^{\circ} \\
& \Delta \lambda=\sum_{j=1}^{8} \Delta \lambda_{j}=1^{\circ}=\pi / 180=0.0174532925199432957692369 \text { radians } \\
& \text { Eq 110. } A \cong \sum_{i=1}^{8}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right)\left[\sum_{j=1}^{8}\left(\frac{\rho\left(\varphi_{j}\right)+\rho\left(\varphi_{j-1}\right)}{2} \Delta \lambda_{j}\right)\right] \\
& \cong\left[\sum_{i=1}^{8}\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right)\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2} \Delta \lambda\right)\right] \\
&\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2} \Delta \varphi_{i}\right)=\operatorname{Height} \text { of strip between } \varphi_{i} \text { and } \varphi_{i-1} . \Delta \varphi_{i}=(1 / 8)^{\circ} \text { as radians } \\
&\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2} \Delta \lambda\right)=\text { Length of strip between } \varphi_{i} \text { and } \varphi_{i-1} . \Delta \lambda=1^{\circ} \text { as radians }
\end{aligned}
$$

The corresponding angle in radians are $0.00000,0.002181,0.004363,0.006544, .008726,0.010908$, $0.013089,0.015271,0.017453$.

The final value for the area of a degree square in latitude and longitude (along the equator) is $12,308.814$ square kilometers. This is slightly different from the information on lengths of degrees of latitude and longitude. A degree of longitude $(\lambda)$ at latitude $\varphi=0^{\circ}$ is 111.319490 km and at latitude $\varphi=1^{\circ}$ is 111.31838 km for an average width is 111.31893 , which implies that on a flat surface, the trapezoid would have an area of $12,309.023$ which is about 0.2 square kilometers too large. In a plane the average is based on a linear growth, but on the ellipsoid the average is mainly associated to the $\cos \varphi$ which is near flat near $\varphi=0$ which goes linear near $90^{\circ}$ (i.e. near the pole). So, the actual area (as latitude increases down the columns below the rapidity of change increases as the squares moves nearer the pole) is slightly larger than a planar approximation.

Table 3. Area of $1^{\circ}$ Latitude by $1^{\circ}$ Longitude at the Equator via Squares (sq. meters)

| Lat $\downarrow$ | $\begin{gathered} \text { Long } \rightarrow \\ .000 \end{gathered}$ | . 125 | . 250 | . 375 | . 500 | . 625 | . 750 | . 875 | 1.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 000 | $\begin{gathered} 192,329,72 \\ 9.221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,72 \\ 9.221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,72 \\ 9.221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,729 \\ .221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,729 \\ .221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,729 \\ .221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,729 \\ .221821 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,729 \\ .221821 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,637,833 . \\ 77457 \end{gathered}$ |
| . 125 | $\begin{gathered} 192,330,23 \\ 6.673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,23 \\ 6.673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,23 \\ 6.673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,236 \\ .673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,236 \\ .673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,236 \\ .673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,236 \\ .673325 \\ \hline \end{gathered}$ | $\begin{gathered} 192,330,236 \\ .673325 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,641,893 . \\ 38660 \end{gathered}$ |
| . 250 | $\begin{gathered} 192,329,84 \\ 7.085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,84 \\ 7.085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,84 \\ 7.085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,847 \\ .085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,847 \\ .085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,847 \\ .085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,847 \\ .085907 \\ \hline \end{gathered}$ | $\begin{gathered} 192,329,847 \\ .085907 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1,538,638,776 . \\ 68726 \end{gathered}$ |
| . 375 | $\begin{gathered} 192,328,56 \\ 0.440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,56 \\ 0.440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,56 \\ 0.440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,560 \\ .440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,560 \\ .440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,560 \\ .440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,560 \\ .440212 \\ \hline \end{gathered}$ | $\begin{gathered} 192,328,560 \\ .440212 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,628,483 . \\ 52170 \end{gathered}$ |
| . 500 | $\begin{gathered} 192,326,37 \\ 6.720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,37 \\ 6.720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,37 \\ 6.720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,376 \\ .720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,376 \\ .720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,376 \\ .720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,376 \\ .720375 \\ \hline \end{gathered}$ | $\begin{gathered} 192,326,376 \\ .720375 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,611,013 . \\ 76300 \end{gathered}$ |
| . 625 | $\begin{gathered} 192,323,29 \\ 5.914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,29 \\ 5.914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,29 \\ 5.914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,295 \\ .914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,295 \\ .914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,295 \\ .914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,295 \\ .914023 \\ \hline \end{gathered}$ | $\begin{gathered} 192,323,295 \\ .914023 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,586,367 . \\ 31218 \end{gathered}$ |
| . 750 | $\begin{gathered} 192,319,31 \\ 8.012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,31 \\ 8.012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,31 \\ 8.012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,318 \\ .012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,318 \\ .012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,318 \\ .012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,318 \\ .012272 \\ \hline \end{gathered}$ | $\begin{gathered} 192,319,318 \\ .012272 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1,538,554,544 . \\ 09818 \end{gathered}$ |
| . 875 | $\begin{gathered} 192,314,44 \\ 3.009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,44 \\ 3.009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,44 \\ 3.009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,443 \\ .009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,443 \\ .009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,443 \\ .009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,443 \\ .009734 \\ \hline \end{gathered}$ | $\begin{gathered} 192,314,443 \\ .009734 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1,538,515,544 . \\ 07788 \end{gathered}$ |
| 1.00 |  |  |  |  |  |  |  |  |  |
| Sum | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 1,538,601,8 \\ 07.07767 \\ \hline \end{gathered}$ | $\begin{gathered} 12,308,814,45 \\ 6.6214 \end{gathered}$ |

Each square $=\left(\frac{\rho\left(\varphi_{i}\right)+\rho\left(\varphi_{i-1}\right)}{2}\right)\left(\frac{M\left(\varphi_{i}\right)+M\left(\varphi_{i-1}\right)}{2}\right)(\Delta \lambda)(\Delta \varphi)$
Table 4. Area of $1^{\circ}$ Latitude by $1^{\circ}$ Longitude at the Equator via Stripes (sq. meters)

| Latitude in <br> radians | Average <br> $\mathbf{M ( p )}$ | Average <br> $\boldsymbol{\rho} \mathbf{\varphi} \boldsymbol{\varphi}$ | Stripe <br> Height | Stripe Length | Area of Row |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0000000 | $6,335,439.32729282$ | $6,378,137.0000000$ | $13,821.78480800$ | $111,352.96452167$ | $1,538,637,833.77457$ |
| 0.00218166 | $6,335,439.63009043$ | $6,378,168.39746324$ | $13,821.78612920$ | $111,351.78018338$ | $1,538,641,893.38660$ |
| 0.00436332 | $6,335,440.53847765$ | $6,378,169.43746257$ | $13,821.78877157$ | $111,348.59284744$ | $1,538,638,776.68726$ |
| 0.00654498 | $6,335,442.05243760$ | $6,378,140.11932799$ | $13,821.79273506$ | $111,342.41803770$ | $1,538,628,483.52170$ |
| 0.00872665 | $6,335,444.17194220$ | $6,378,080.44253395$ | $13,821.79801961$ | $111,332.26756270$ | $1,538,611,013.76300$ |
| 0.01090831 | $6,335,446.89695210$ | $6,377,990.40669941$ | $13,821.80462511$ | $111,317.15280954$ | $1,538,586,367.31218$ |
| 0.01308997 | $6,335,450.22741673$ | $6,377,870.01158780$ | $13,821.81255144$ | $111,296.10221165$ | $1,538,554,544.09818$ |
| 0.01527163 | $6,335,454.16327427$ | $6,377,719.25710712$ | $13,821.82179845$ | $110,943.09955475$ | $1,538,515,544.07787$ |
| 0.01745329 |  |  |  | $12,308,814,456.6214$ |  |
|  |  |  |  |  |  |

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[^0]:    ${ }^{1}$ The nominal measure of position with respect to these lines are expressed in angles, for latitude measured by the angular direction of the local surface vertical as it crosses the equatorial plane. For longitude this is the central angle for the reference ellipsoid, as a rotation parallel to the equatorial plane with respect to the prime meridian. If the ellipsoid is a not a sphere the latitude " $\varphi$ " is not the same as the central angle " $\psi$ ".

